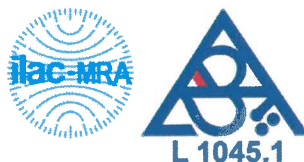




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ČSN EN ISO/IEC 17025:2018

Strojírenský zkušební ústav, s.p. Zkušební laboratoř
(Engineering Test Institute, Public Enterprise, Testing Laboratory)
Hudcova 424/56b, Medlánky, 621 00 Brno

Page 1 of 33



TEST REPORT

39-17758/T

Product: Outdoor Air/Water Heat pump - monobloc

Type designation: TAHMV12S A

Customer: Guangdong Tongyi Heat Pump Science and Technology Corp.
Room 2001-2010, 20/F, No.159 Middle Qiaozhong Road
510163 Liwan District, Guangzhou
CHINA

Manufacturer: Guangdong Tongyi Heat Pump Science and Technology Corp.
Room 2001-2010, 20/F, No.159 Middle Qiaozhong Road
510163 Liwan District, Guangzhou
CHINA

Report issue date: 2024-07-18

Distribution list: 1 copy to the Customer
1 copy to the Engineering Test Institute

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SP-2021-000012_1_12

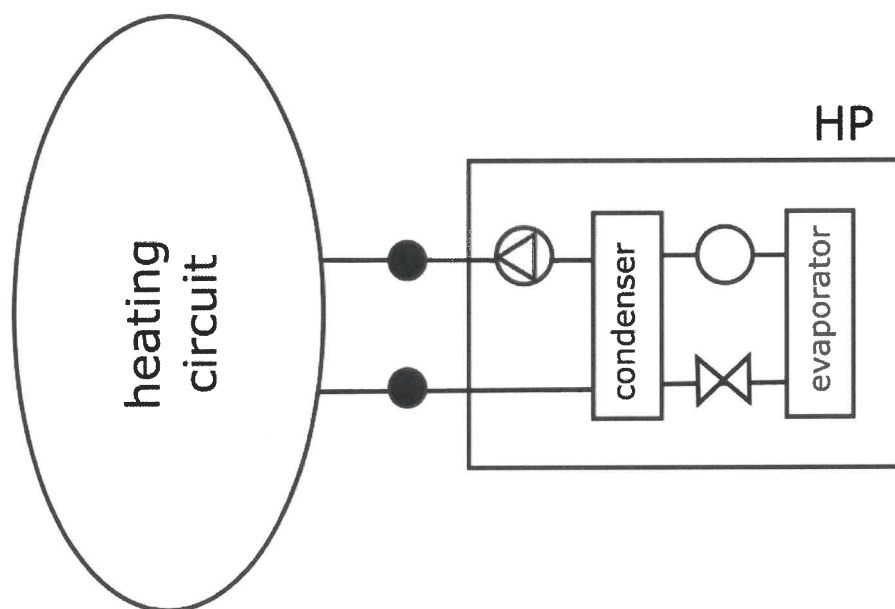
I. Description of product tested

The Heat pump **TAH MV12S A** supplied by the company **Guangdong Tongyi Heat Pump Science and Technology Corp.** is structurally adapted to operate in air/water system. Device is designed as monobloc placed outdoor. Refrigerant R32 is used with charge 2.2 kg. Power supply is a three-phase. Heat pump is able to work in heating and cooling mode. Heat pump is working with fixed flow rate.

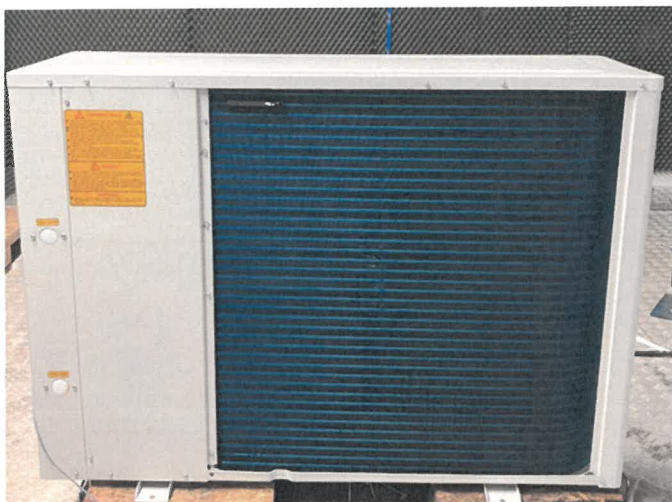
Main components of the outdoor unit **TAH MV12S A**:

- Serial number NETAH MV12SBWY12SX000288
- Cuboid shape with dimensions 1260 × 425 × 865 mm (W × D × H)
- Frame and casing made of varnished steel sheets
- L-shaped evaporator, 3 rows, dimensions 840 × 20 × 1140 mm (W × D × H), spacing 2 mm
- Plate condenser, dimensions 70 × 30 × 310 mm (W × D × H) including insulation
- Plate condenser, dimensions 140 × 140 × 340 mm (W × D × H) including insulation
- Compressor Panasonic 9KD420ZAA2J
- Refrigerant R32 (2.2 kg)
- Refrigerant accumulator
- Axial fan Ø560 mm
- DC motor ZSFN-310-8-85F
- Circulation pump SHIMGE
- Paddle flow switch ACOL
- Expansion tank 2L ACOL
- Pressure sensors
- Temperature sensors
- Refrigerant pipes

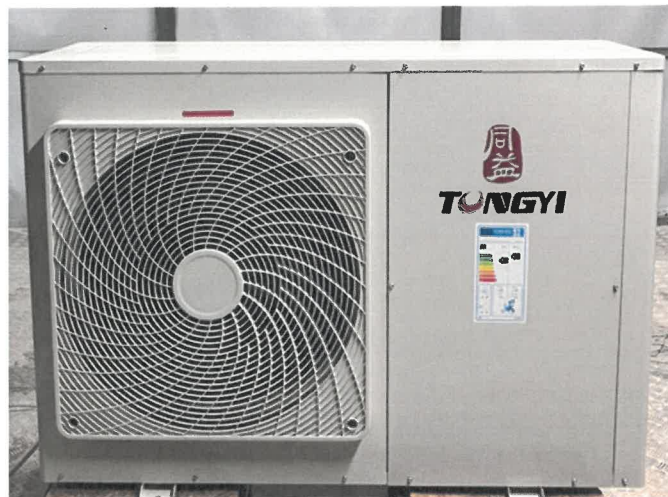
Scheme:



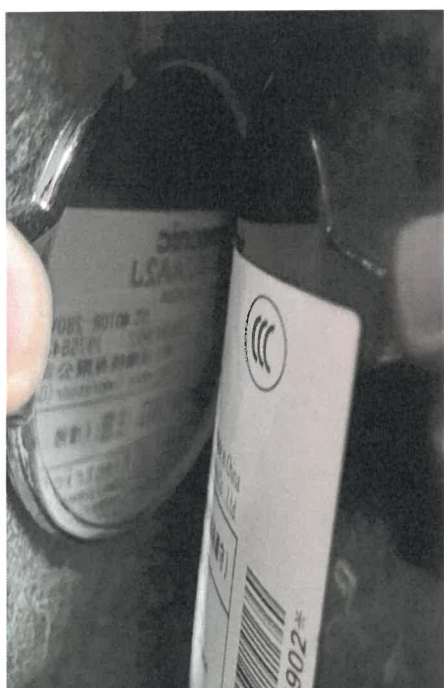
Photodocumentation:



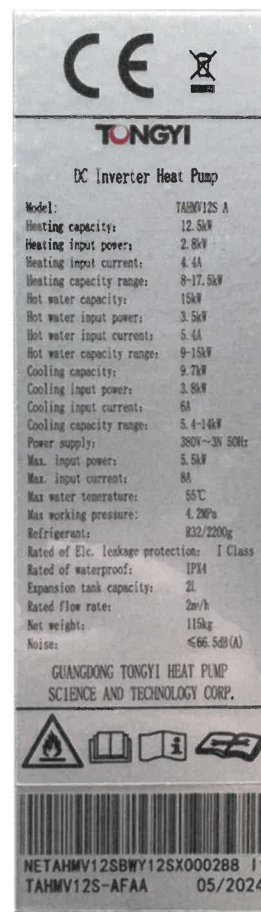
Heat pump TAHMV12S A – outdoor unit
– Front view –



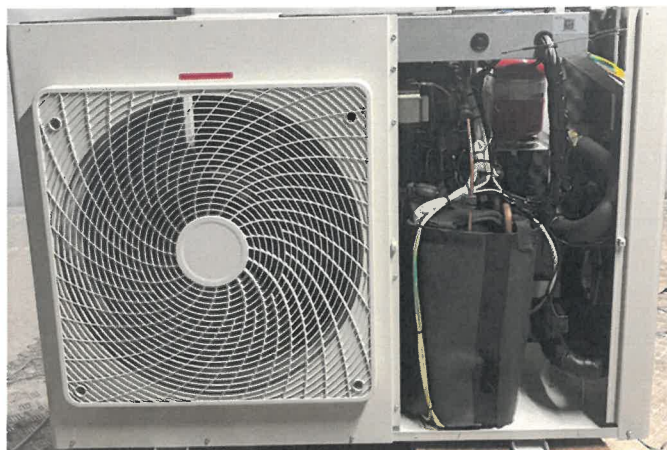
Heat pump TAHMV12S A – outdoor unit
– Back view –



Heat pump TAHMV12S A – outdoor unit
– Compressor label –



Heat pump TAHMV12S A – outdoor unit
– Label –



Heat pump TAHMV12S A – outdoor unit
– Without cover –

II. Sample tested

SZU reg. no.	Product name	Date of submission
1212.24.40194.001	TAHMOV12S	2024-06-19

The visual inspection, tests and verification were carried out by Ing. Alexandr Jordanov and Ing. Dominik Šedivý, Ph.D. at the test station of SZU.

The tests were performed using measuring and testing equipment with valid calibration.

III. Measuring and test equipment:

No.	Description	Inventory number
1.	Electrical energy meter	022370/1
2.	Digital watt meter	MaR01/EM01
3.	Flow meter Krohne Optiflux	022370/5
4.	Barometer	022370/7
5.	Differential pressure gauge	MaR01_TI
6.	Temperature-humidity meter HC2-IC305	022370/10
7.	Temperature-humidity meter HC2-IC305	022370/11 022370/12
8.	Thermometers	022370/13

No.	Test objective	Requirement	Method of test	Documentation	Test evaluation/ verification *
1.	Rating conditions	–	ČSN EN 14511-2:2023 ČSN EN 14511-3:2023	Page No. 6	x
2.	Seasonal performance tests and SCOP calculation – Low temperature application	–	ČSN EN 14511-3:2023 ČSN EN 14825:2023	Page No. 7-13	x
3.	Seasonal performance tests and SCOP calculation – Medium temperature application	–	ČSN EN 14511-3:2023 ČSN EN 14825:2023	Page No. 14-20	x

*) Evaluation / statement of conformity:

+ Requirement fulfilled
0Not applicable

- Requirement not fulfilled
xNot evaluated

The stated extended measurement uncertainties are calculated as a factor of the measurement uncertainty and the extension coefficient $k=2$, corresponding to the coverage certainty of 95% as regards standard classification.

SP-2021-000012 1 12

Test objective:	Rating conditions
Exact name of the test procedure:	1.37 - Tests of leakage, pressure resistance, thermal and technical parameters, combustion efficiency, safety functions
Test method:	ČSN EN 14511-2:2023, ČSN EN 14511-3:2023
Sample tested:	Heat pump TAHMV12S A
Measuring equipment used:	see Chapter III

Specification of the assessment condition		A7/W35	A7/W55
Date of testing		2024-07-09	2024-07-09
Transient test procedure	YES / NO	NO	NO
Average defrost time of 1 cycle	[min]	–	–
Average time of 1 cycle	[min]	–	–
Calculation time	[min]	70.0	70.0
Output heating water – temperature calculation	[°C]	34.98	55.03
Input heating water – temperature calculation	[°C]	29.93	46.98
Output heating water temperature	[°C]	34.98	55.03
Input heating water temperature	[°C]	29.93	46.98
Air temperature – dry bulb temperature	[°C]	6.89	6.93
Air temperature – wet bulb temperature	[°C]	5.83	5.88
Relative humidity	[%]	86.03	86.06
Barometric pressure	[kPa]	98.782	98.627
Ambient temperature	[°C]	7.14	7.23
Secondary circuit pressure difference	[kPa]	98.425	98.374
Efficiency of the secondary liquid pump	[–]	0.441	0.437
Volume flow rate of heating water	[m ³ ·h ⁻¹]	2.0634	1.2744
Density of heating water	[kg·m ⁻³]	994.0	985.8
Specific heat capacity of heating water	[kJ·kg ⁻¹ ·K ⁻¹]	4.175	4.179
Voltage	[V]	399.41	398.99
Total current	[A]	12.76	17.94
Overall power input	[kW]	2.542	3.759
Capacity correction of sec. liquid pump	[W]	62.61	58.17
Power input correction of sec. liquid pump	[W]	95.51	87.45
Heating capacity – heating water	[kW]	11.996	11.779
Corrected heating capacity – heating water	[kW]	11.933	11.721
Uncertainty of corrected heating capacity	[kW]	± 0.203	± 0.126
Effective electric power input	[kW]	2.446	3.672
COP	[–]	4.878	3.192
Uncertainty of COP	[–]	± 0.085	± 0.035
Control settings	[Hz]	45	42
Circulation pump settings – heating water	[%]	100	100

Test objective:	Seasonal performance tests and SCOP calculation – Low temperature application
Exact name of the test procedure:	1.37 - Tests of leakage, pressure resistance, thermal and technical parameters, combustion efficiency, safety functions
Test method:	ČSN EN 14511-3:2023, ČSN EN 14825:2023
Sample tested:	Heat pump TAHMV12S A
Measuring equipment used:	see Chapter III

Design			Air / water – monobloc				
Conditions specification according to ČSN 14825:2023	to EN	Temperature application				Low (reference water temperature 35 °C)	
		Reference heating season				Average	
		Outlet water temperature - indoor heat exchanger				Variable	
		Compressor speed control				Variable	
		Water flow rate – primary circuit				–	
		Water flow rate – secondary circuit				Fixed	
Seasonal heating efficiency	space energy	Heating	Average	ηs		183.2	%
			Warmer	ηs		–	%
			Colder	ηs		–	%
Seasonal efficiency according to ČSN 14825:2023	EN	Heating	Average	SCOP		4.66	–
			Warmer	SCOP		–	–
			Colder	SCOP		–	–
Function	Cooling					Yes	
	Heating	Yes	Reference heating season	Average	Yes		
				Warmer	–		
				Colder	–		
Full heating load	Cooling		Pdesignc		–	kW	
	Heating	Average	Pdesignh		10.20	kW	
		Warmer	Pdesignh		–	kW	
		Colder	Pdesignh		–	kW	
Bivalent temperatures	Heating	Average	Tbivalent		-7	°C	
		Warmer	Tbivalent		–	°C	
		Colder	Tbivalent		–	°C	
Operation temperatures limit	Heating	Average	TOL		-10	°C	
		Warmer	TOL		–	°C	
		Colder	TOL		–	°C	
Seasonal consumption according to ČSN EN 14825:2023	power to	Cooling		QCE		–	kWh
		Heating	Average	QHE		4524	kWh
			Warmer	QHE		–	kWh
			Colder	QHE		–	kWh
Modes other than „active mode“			Off mode		POFF	52.4	W
			Thermostat off mode		PTo	53.7	W
			Standby mode		PSB	52.4	W
			Crankcase heater mode		PCK	0.0	W

Calculation of SCOP according to ČSN EN 14825:2023:

Number of hours used for calculation of reference SCOP (Annex B – Table B. 2, B. 3)

- For reversible heat pumps and reference heating season „A“ = average

H _{HE}	2066	[h]
H _{TO}	178	[h]
H _{SB}	0	[h]
H _{CK}	178	[h]
H _{OFF}	0	[h]

Measured data:

P _{TO}	0.0537	[kW]
P _{SB}	0.0524	[kW]
P _{CK}	0.0000	[kW]
P _{OFF}	0.0524	[kW]
P _{designh}	10.20	[kW]
SCOP _{ON}	4.67	[-]

Coefficient and correction:

F(1)	3	[%]
F(2)	0	[%]
CC	2.5	[-]

Calculation of SCOP:

7.3 Calculation of the reference annual heating demand (Q_H)

$$Q_H = P_{\text{designh}} \cdot H_{\text{HE}} \quad [\text{kWh}]$$

$$Q_H = 10.20 \cdot 2066 = \mathbf{21065} \quad [\text{kWh}]$$

7.4 Calculation of the annual electricity consumption (Q_{HE})

$$Q_{\text{HE}} = Q_H / \text{SCOP}_{\text{on}} + H_{\text{TO}} \cdot P_{\text{TO}} + H_{\text{SB}} \cdot P_{\text{SB}} + H_{\text{CK}} \cdot P_{\text{CK}} + H_{\text{OFF}} \cdot P_{\text{OFF}} \quad [\text{kWh}]$$

$$Q_{\text{HE}} = 21065 / 4.67 + 178 \cdot 0.0537 + 0 \cdot 0.0524 + 178 \cdot 0 + 0 \cdot 0.0524 = \mathbf{4524} \quad [\text{kWh}]$$

7.2 General formula for calculation of reference SCOP

$$\text{SCOP} = Q_H / Q_{\text{HE}} \quad [-]$$

$$\text{SCOP} = 21065 / 4524 = \mathbf{4.66} \quad [-]$$

7.1 Calculation of the seasonal space heating efficiency η_s

$$\Sigma F(i) = F(1) + F(2) \quad [-]$$

$$\Sigma F = 0.03 + 0 = 0.03 \quad [-]$$

$$\eta_s = 1 / \text{CC} \cdot \text{SCOP} - \Sigma F(i) \quad [-]$$

$$\eta_s (A) = (1 / 2.5) \cdot 4.66 - 0.03 = \mathbf{1.832} \quad [-]$$

Temperature level		Low (reference water temperature 35 °C)		
Reference heating season		„A“ = average ($T_{\text{designh}} = -10\text{ °C}$)		
Assessment condition		B	C	D
Specification of the assessment condition		A2/W30	A7/W28.24	A12/W26.48
Date of testing		2024-07-10	2024-07-10	2024-07-16
Transient test procedure	YES / NO	NO	NO	NO
Average defrost time of 1 cycle	[min]	–	–	–
Average time of 1 cycle	[min]	–	–	–
Calculation time	[min]	70.0	70.0	70.0
Output heating water – temperature calculation	[°C]	29.97	28.25	26.48
Input heating water – temperature calculation	[°C]	27.57	25.49	23.30
Output heating water temperature	[°C]	29.97	28.25	26.48
Input heating water temperature	[°C]	27.57	25.49	23.30
Air temperature – dry bulb temperature	[°C]	2.05	7.03	11.89
Air temperature – wet bulb temperature	[°C]	1.00	5.95	10.82
Relative humidity	[%]	83.06	85.77	88.12
Barometric pressure	[kPa]	98.441	98.306	98.147
Ambient temperature	[°C]	1.93	7.09	11.98
Secondary circuit pressure difference	[kPa]	60.236	59.882	57.087
Efficiency of the secondary liquid pump	[-]	0.348	0.348	0.344
Volume flow rate of heating water	[m ³ ·h ⁻¹]	2.0551	2.0603	2.0550
Density of heating water	[kg·m ⁻³]	995.5	996.0	996.5
Specific heat capacity of heating water	[kJ·kg ⁻¹ ·K ⁻¹]	4.176	4.176	4.177
Voltage	[V]	399.72	399.93	399.65
Total current	[A]	6.99	6.78	5.90
Overall power input	[kW]	1.297	1.194	1.064
Capacity correction of sec. liquid pump	[W]	64.425	64.284	62.219
Power input correction of sec. liquid pump	[W]	98.81	98.55	94.81
Heating capacity – heating water	[kW]	5.685	6.554	7.552
Corrected heating capacity – heating water	[kW]	5.620	6.489	7.490
Uncertainty of corrected heating capacity	[kW]	± 0.202	± 0.202	± 0.202
Effective electric power input	[kW]	1.198	1.095	0.969
COP	[-]	4.692	5.925	7.727
Uncertainty of COP	[-]	± 0.169	± 0.186	± 0.210
Control settings	[Hz]	25	25	25
Circulation pump settings – heating water	[%]	100	100	100

Temperature level		Low (reference water temperature 35 °C)	
Reference heating season		„A“ = average ($T_{\text{designh}} = -10\text{ °C}$)	
Assessment condition		TOL(E)	A, Tbiv(F)
Specification of the assessment condition		A-10/W35	A-7/W34
Date of testing		2024-07-16	2024-07-10
Transient test procedure	YES / NO	NO	YES
Average defrost time of 1 cycle	[min]	–	5.6
Average time of 1 cycle	[min]	–	105.3
Calculation time	[min]	70.0	105.3
Output heating water – temperature calculation	[°C]	35.01	33.19
Input heating water – temperature calculation	[°C]	30.93	29.36
Output heating water temperature	[°C]	35.01	34.03
Input heating water temperature	[°C]	30.93	29.64
Air temperature – dry bulb temperature	[°C]	-9.98	-7.15
Air temperature – wet bulb temperature	[°C]	-10.96	-8.15
Relative humidity	[%]	68.99	73.73
Barometric pressure	[kPa]	98.078	98.551
Ambient temperature	[°C]	-10.26	-6.85
Secondary circuit pressure difference	[kPa]	57.777	60.427
Efficiency of the secondary liquid pump	[-]	0.345	0.348
Volume flow rate of heating water	[m ³ ·h ⁻¹]	2.0544	2.0536
Density of heating water	[kg·m ⁻³]	994.0	994.5
Specific heat capacity of heating water	[kJ·kg ⁻¹ ·K ⁻¹]	4.175	4.175
Voltage	[V]	399.05	399.05
Total current	[A]	15.31	15.01
Overall power input	[kW]	3.162	3.090
Capacity correction of sec. liquid pump	[W]	62.691	64.530
Power input correction of sec. liquid pump	[W]	95.66	99.00
Heating capacity – heating water	[kW]	9.651	9.084
Corrected heating capacity – heating water	[kW]	9.589	9.020
Uncertainty of corrected heating capacity	[kW]	± 0.202	± 0.202
Effective electric power input	[kW]	3.067	2.991
COP	[-]	3.127	3.015
Uncertainty of COP	[-]	± 0.066	± 0.068
Control settings	[Hz]	56	56
Circulation pump settings – heating water	[%]	100	100

Data for SCOP calculation

- Low temperature application (reference water temperature 35 °C)
- Reference heating season „A“ – average

	Outdoor heat exchanger	Indoor heat exchanger	Part load ratio	Part load	DC Declared capacity	COPd at declared capacity	Cdh degradation coefficient	CR	COPbin (Tj)	Eff. power input of compressor off state
	Outdoor air inlet	Outlet water temperature								
	[°C]	[°C]	[%]	[kW]	[kW]	[-]	[-]	[-]	[-]	[kW]
A	-7	34.00	88.46	9.02	9.020	3.015	0.900	1.00	3.015	–
B	2	30.00	53.85	5.49	5.620	4.692	0.900	1.00	4.692	–
C	7	28.24	34.62	3.53	6.496	5.925	0.951	0.45	5.690	0.0537
D	12	26.48	15.38	1.57	7.490	7.727	0.945	0.21	6.391	0.0537
TOL (E)	-10	35.00	100.00	10.20	9.589	3.127	0.900	1.00	3.127	–
Tbiv (F)	-7	34.00	88.46	9.02	9.020	3.015	0.900	1.00	3.015	–

Adaption of water temperature – according to ČSN EN 14825:2023, Annex E

- Low temperature application (reference water temperature 35 °C)
- Reference season „A“ – average
- Condition D
- Fixed water flow rate – secondary circuit

General formulas and derivation:

$$\begin{aligned}
 t_{\text{outlet, average}} &= t_{\text{inlet, capacity test}} + (t_{\text{outlet, capacity test}} - t_{\text{inlet, capacity test}}) \cdot CR & [^{\circ}\text{C}] \\
 t_{\text{outlet, average}} &= t_{\text{inlet, capacity test}} + (\Delta t) \cdot CR & [^{\circ}\text{C}] \\
 t_{\text{outlet, average}} &= t_{\text{outlet, capacity test}} - \Delta t + \Delta t \cdot CR & [^{\circ}\text{C}] \\
 t_{\text{outlet, capacity test}} &= t_{\text{outlet, average}} + \Delta t - \Delta t \cdot CR & [^{\circ}\text{C}]
 \end{aligned}$$

For fixed flow:

$$\Delta t = \text{Declared capacity} / \text{Declared capacity}_{\text{standard rating conditions A7W35}} \cdot 5$$

$$CR \cdot \Delta t = \text{Part load} / \text{Declared capacity} \cdot \text{Declared capacity} / \text{Declared capacity}_{\text{standard rating conditions A7W35}} \cdot 5$$

$$CR \cdot \Delta t = \text{Part load} / \text{Declared capacity}_{\text{standard rating conditions A7W35}} \cdot 5$$

$$t_{\text{outlet, capacity test, fixed flow}} = t_{\text{outlet, average}} + \text{Declared capacity} / \text{Declared capacity}_{\text{standard rating conditions A7W35}} \cdot 5 - \text{Part load} / \text{Declared capacity}_{\text{standard rating conditions A7W35}} \cdot 5$$

$$t_{\text{outlet, capacity test, fixed flow}} = t_{\text{outlet, average}} + 5 / \text{Declared capacity}_{\text{standard rating conditions A7W35}} \cdot (\text{Declared capacity} - \text{Part load})$$

Measured data:

$t_{\text{outlet, average}}$	24.00	[°C]
Declared capacity	7.490	[kW]
Declared capacity _{standard rating condition A7/W35}	11.933	[kW]
Part load	1.57	[kW]

Calculation of water temperature

$$t_{\text{outlet, capacity test, fixed flow}} = 24 + 5 / 11.933 \cdot (7.490 - 1.570) = \underline{26.48} \quad [^{\circ}\text{C}]$$

Calculation SCOP, SCOP_{on}, SCOP_{net}

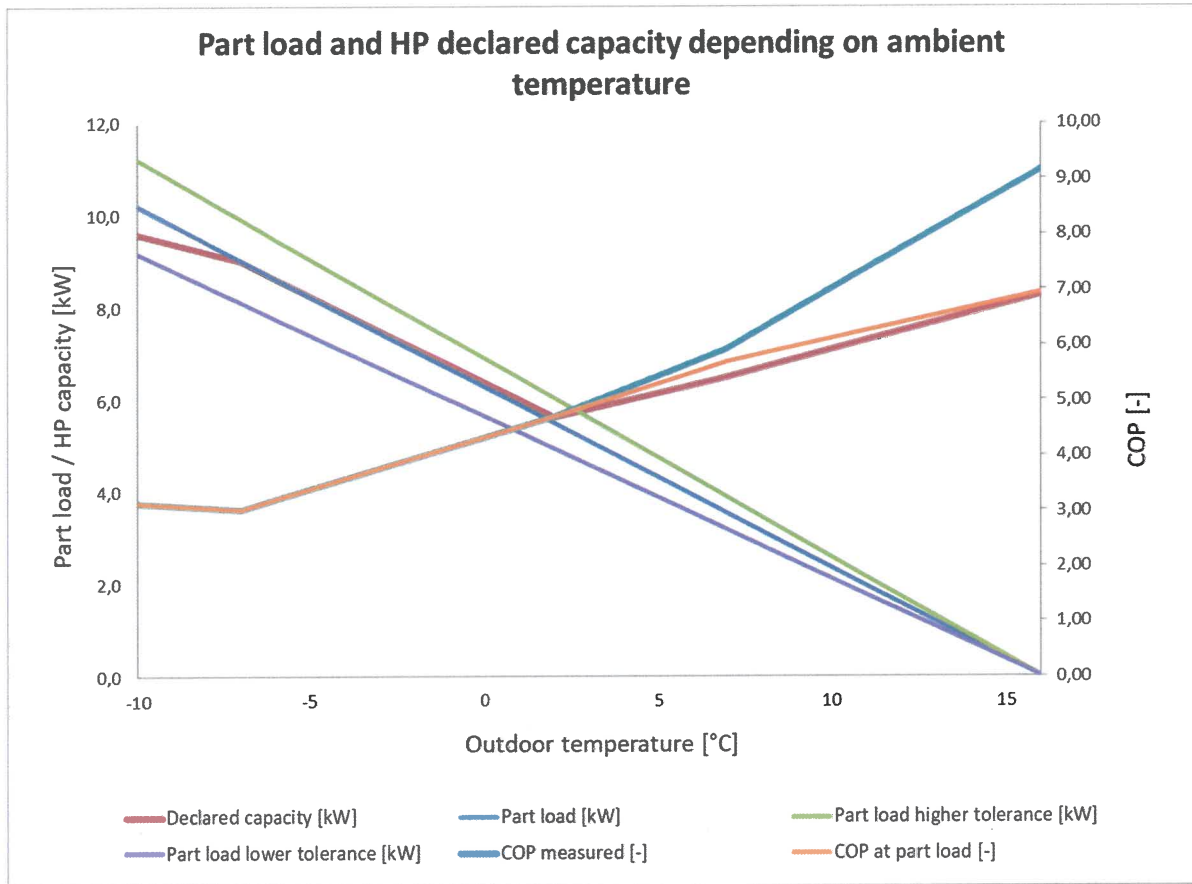
- Low temperature application (reference water temperature 35 °C)
- Reference heating season „A“ – average

	Bin	Outdoor temp. (dry bulb)	Hours	Part load ratio	Heat load	Capacity of HP	Heat load covered by heat pump	Resistive heat elbu (Tj)	Annual resistive heat	COPbin (Tj)	Annual heating demand	Annual power input including electric back up heating	Net annual heating capacity	Net annual power input without electric back up heating
	j	Tj	hj		Ph(Tj)			elbu(Tj)	hj x elbu(Tj)	COPbin (Tj)	hj x Ph(Tj)		hj x (Ph(Tj) - elbu(Tj))	
	[-]	[°C]	[h]	[%]	[kW]	[kW]	[kW]	[kW]	[kWh]	[-]	[kWh]	[kWh]	[kWh]	[kWh]
TOL(E)	21	-10	1	100.00	10.20	9.59	9.59	0.61	0.61	3.13	10	4	10	3
	22	-9	25	96.15	9.80	9.40	9.40	0.40	10.12	3.09	245	86	235	76
	23	-8	23	92.31	9.41	9.21	9.21	0.20	4.66	3.05	216	74	212	69
A, T_{biv} (F)	24	-7	24	88.46	9.02	9.02	9.02	0.00	0.00	3.02	216	72	216	72
	25	-6	27	84.62	8.63	8.64	8.63	0.00	0.00	3.20	233	73	233	73
	26	-5	68	80.77	8.24	8.26	8.24	0.00	0.00	3.39	560	165	560	165
	27	-4	91	76.92	7.84	7.89	7.84	0.00	0.00	3.57	714	200	714	200
	28	-3	89	73.08	7.45	7.51	7.45	0.00	0.00	3.76	663	176	663	176
	29	-2	165	69.23	7.06	7.13	7.06	0.00	0.00	3.95	1165	295	1165	295
	30	-1	173	65.38	6.67	6.75	6.67	0.00	0.00	4.13	1153	279	1153	279
	31	0	240	61.54	6.27	6.38	6.27	0.00	0.00	4.32	1506	349	1506	349
	32	1	280	57.69	5.88	6.00	5.88	0.00	0.00	4.51	1647	366	1647	366
B	33	2	320	53.85	5.49	5.62	5.49	0.00	0.00	4.69	1757	374	1757	374
	34	3	357	50.00	5.10	5.80	5.10	0.00	0.00	4.89	1820	372	1820	372
	35	4	356	46.15	4.71	5.97	4.71	0.00	0.00	5.09	1675	329	1675	329
	36	5	303	42.31	4.31	6.15	4.31	0.00	0.00	5.29	1307	247	1307	247
	37	6	330	38.46	3.92	6.32	3.92	0.00	0.00	5.49	1294	236	1294	236
C	38	7	326	34.62	3.53	6.50	3.53	0.00	0.00	5.69	1151	202	1151	202
	39	8	348	30.77	3.14	6.70	3.14	0.00	0.00	5.83	1092	187	1092	187
	40	9	335	26.92	2.75	6.89	2.75	0.00	0.00	5.97	920	154	920	154
	41	10	315	23.08	2.35	7.09	2.35	0.00	0.00	6.11	741	121	741	121
	42	11	215	19.23	1.96	7.29	1.96	0.00	0.00	6.25	422	67	422	67
D	43	12	169	15.38	1.57	7.49	1.57	0.00	0.00	6.39	265	41	265	41
	44	13	151	11.54	1.18	7.69	1.18	0.00	0.00	6.53	178	27	178	27
	45	14	105	7.69	0.78	7.89	0.78	0.00	0.00	6.67	82	12	82	12
	46	15	74	3.85	0.39	8.09	0.39	0.00	0.00	6.81	29	4	29	4
	Σ		4910							Σ	21061	4514	21046	4498

SCOP _{on}	4.67	SCOP _{net}	4.68
		SCOP	4.66

Part load performance diagram

- Low temperature application (reference water temperature 35 °C)
- Reference heating season „A“ – average



Test objective:	Seasonal performance tests and SCOP calculation – Medium temperature application
Exact name of the test procedure:	1.37 - Tests of leakage, pressure resistance, thermal and technical parameters, combustion efficiency, safety functions
Test method:	ČSN EN 14511-3:2023, ČSN EN 14825:2023
Sample tested:	Heat pump TAHMV12S A
Measuring equipment used:	see Chapter III

Design			Air / water – monobloc			
Conditions specification according to ČSN 14825:2023	to EN	Temperature application			Medium (reference water temperature 55 °C)	
		Reference heating season			Average	
		Outlet water temperature - indoor heat exchanger			Variable	
		Compressor speed control			Variable	
		Water flow rate – primary circuit			–	
		Water flow rate – secondary circuit			Fixed	
Seasonal space heating efficiency	Heating	Average	ηs		138.6	%
		Warmer	ηs		–	%
		Colder	ηs		–	%
Seasonal efficiency according to ČSN 14825:2023	Heating	Average	SCOP		3.54	–
		Warmer	SCOP		–	–
		Colder	SCOP		–	–
Function	Cooling					Yes
	Heating	Yes	Reference heating season	Average	Yes	
				Warmer	–	
				Colder	–	
Full heating load	Cooling		Pdesignc		–	kW
	Heating	Average	Pdesignh		10.96	kW
		Warmer	Pdesignh		–	kW
		Colder	Pdesignh		–	kW
Bivalent temperatures	Heating	Average	Tbivalent		-7	°C
		Warmer	Tbivalent		–	°C
		Colder	Tbivalent		–	°C
Operation limit temperatures	Heating	Average	TOL		-10	°C
		Warmer	TOL		–	°C
		Colder	TOL		–	°C
Seasonal power consumption according to ČSN EN 14825:2023	Cooling		QCE		–	kWh
	Heating	Average	QHE		6406	kWh
		Warmer	QHE		–	kWh
		Colder	QHE		–	kWh
Modes other than „active mode“		Off mode			POFF	52.4 W
		Thermostat off mode			PTo	54.0 W
		Standby mode			PSB	52.4 W
		Crankcase heater mode			PCK	0.0 W

Calculation of SCOP according to ČSN EN 14825:2023:

Number of hours used for calculation of reference SCOP (Annex B – Table B. 2, B. 3)

- For reversible heat pumps and reference heating season „A“ = average

H _{HE}	2066	[h]
H _{TO}	178	[h]
H _{SB}	0	[h]
H _{CK}	178	[h]
H _{OFF}	0	[h]

Measured data:

P _{TO}	0.0540	[kW]
P _{SB}	0.0524	[kW]
P _{CK}	0.0000	[kW]
P _{OFF}	0.0524	[kW]
P _{designh}	10.96	[kW]
SCOP _{ON}	3.54	[-]

Coefficient and correction:

F(1)	3	[%]
F(2)	0	[%]
CC	2.5	[-]

Calculation of SCOP:

7.3 Calculation of the reference annual heating demand (Q_H)

$$Q_H = P_{\text{designh}} \cdot H_{HE} \quad [\text{kWh}]$$

$$Q_H = 10.96 \cdot 2066 = \mathbf{22643} \quad [\text{kWh}]$$

7.4 Calculation of the annual electricity consumption (Q_{HE})

$$Q_{HE} = Q_H / \text{SCOP}_{\text{on}} + H_{TO} \cdot P_{TO} + H_{SB} \cdot P_{SB} + H_{CK} \cdot P_{CK} + H_{OFF} \cdot P_{OFF} \quad [\text{kWh}]$$

$$Q_{HE} = 22643 / 3.54 + 178 \cdot 0.0540 + 0 \cdot 0.0524 + 178 \cdot 0 + 0 \cdot 0.0524 = \mathbf{6406} \quad [\text{kWh}]$$

7.2 General formula for calculation of reference SCOP

$$\text{SCOP} = Q_H / Q_{HE} \quad [-]$$

$$\text{SCOP} = 22643 / 6406 = \mathbf{3.54} \quad [-]$$

7.1 Calculation of the seasonal space heating efficiency η_s

$$\Sigma F(i) = F(1) + F(2) \quad [-]$$

$$\Sigma F = 0.03 + 0 = 0.03 \quad [-]$$

$$\eta_s = 1 / \text{CC} \cdot \text{SCOP} - \Sigma F(i) \quad [-]$$

$$\eta_s (A) = (1 / 2.5) \cdot 3.54 - 0.03 = \mathbf{1.386} \quad [-]$$

Temperature level		Medium (reference water temperature 55 °C)		
Reference heating season		„A“ = average ($T_{designh} = -10\text{ °C}$)		
Assessment condition		B	C	D
Specification of the assessment condition		A2/W42	A7/W37.68	A12/W33.30
Date of testing		2024-07-11	2024-07-11	2024-07-11
Transient test procedure	YES / NO	NO	NO	NO
Average defrost time of 1 cycle	[min]	–	–	–
Average time of 1 cycle	[min]	–	–	–
Calculation time	[min]	70.0	70.0	70.0
Output heating water – temperature calculation	[°C]	42.00	37.70	33.30
Input heating water – temperature calculation	[°C]	37.76	33.40	28.82
Output heating water temperature	[°C]	42.00	37.70	33.30
Input heating water temperature	[°C]	37.76	33.40	28.82
Air temperature – dry bulb temperature	[°C]	2.06	6.93	11.86
Air temperature – wet bulb temperature	[°C]	0.98	5.85	10.78
Relative humidity	[%]	82.70	85.85	88.08
Barometric pressure	[kPa]	98.513	98.442	98.433
Ambient temperature	[°C]	1.91	6.88	11.87
Secondary circuit pressure difference	[kPa]	86.992	87.161	87.380
Efficiency of the secondary liquid pump	[-]	0.339	0.340	0.340
Volume flow rate of heating water	[m ³ ·h ⁻¹]	1.2702	1.2788	1.2772
Density of heating water	[kg·m ⁻³]	991.5	993.1	994.5
Specific heat capacity of heating water	[kJ·kg ⁻¹ ·K ⁻¹]	4.175	4.175	4.175
Voltage	[V]	399.23	399.76	399.91
Total current	[A]	9.68	7.96	7.40
Overall power input	[kW]	1.837	1.478	1.285
Capacity correction of sec. liquid pump	[W]	59.898	60.223	60.275
Power input correction of sec. liquid pump	[W]	90.59	91.18	91.28
Heating capacity – heating water	[kW]	6.202	6.332	6.583
Corrected heating capacity – heating water	[kW]	6.142	6.271	6.523
Uncertainty of corrected heating capacity	[kW]	± 0.125	± 0.126	± 0.126
Effective electric power input	[kW]	1.746	1.386	1.193
COP	[-]	3.518	4.523	5.466
Uncertainty of COP	[-]	± 0.072	± 0.092	± 0.107
Control settings	[Hz]	25	25	25
Circulation pump settings – heating water	[%]	100	100	100

Temperature level		Medium (reference water temperature 55 °C)	
Reference heating season		„A“ = average ($T_{designh} = -10\text{ °C}$)	
Assessment condition		TOL(E)	A, T_{biv}(F)
Specification of the assessment condition		A-10/W55	A-7/W52
Date of testing		2024-07-12	2024-07-11
Transient test procedure	YES / NO	YES	YES
Average defrost time of 1 cycle	[min]	4.4	4.8
Average time of 1 cycle	[min]	120.7	122.8
Calculation time	[min]	120.7	122.8
Output heating water – temperature calculation	[°C]	54.27	51.26
Input heating water – temperature calculation	[°C]	48.10	44.59
Output heating water temperature	[°C]	54.99	52.01
Input heating water temperature	[°C]	48.22	44.68
Air temperature – dry bulb temperature	[°C]	-10.16	-7.00
Air temperature – wet bulb temperature	[°C]	-11.16	-8.04
Relative humidity	[%]	69.56	73.91
Barometric pressure	[kPa]	98.256	98.622
Ambient temperature	[°C]	-10.31	-7.09
Secondary circuit pressure difference	[kPa]	83.253	86.512
Efficiency of the secondary liquid pump	[-]	0.335	0.338
Volume flow rate of heating water	[m ³ ·h ⁻¹]	1.2719	1.2701
Density of heating water	[kg·m ⁻³]	986.2	987.6
Specific heat capacity of heating water	[kJ·kg ⁻¹ ·K ⁻¹]	4.179	4.178
Voltage	[V]	399.23	399.01
Total current	[A]	20.25	19.78
Overall power input	[kW]	4.333	4.180
Capacity correction of sec. liquid pump	[W]	58.324	59.684
Power input correction of sec. liquid pump	[W]	87.74	90.21
Heating capacity – heating water	[kW]	9.028	9.757
Corrected heating capacity – heating water	[kW]	8.969	9.697
Uncertainty of corrected heating capacity	[kW]	± 0.125	± 0.125
Effective electric power input	[kW]	4.245	4.089
COP	[-]	2.113	2.371
Uncertainty of COP	[-]	± 0.030	± 0.031
Control settings	[Hz]	56	56
Circulation pump settings – heating water	[%]	100	100

Data for SCOP calculation

- Medium temperature application (reference water temperature 55 °C)
- Reference heating season „A“ – average

	Outdoor heat exchanger	Indoor heat exchanger	Part load ratio	Part load	DC Declared capacity	COPd at declared capacity	Cdh degradation coefficient	CR	COPbin (Tj)	Eff. power input of compressor off state
	Outdoor air inlet	Outlet water temperature								
	[°C]	[°C]	[%]	[kW]	[kW]	[-]	[-]	[-]	[-]	[kW]
A	-7	52.00	88.46	9.70	9.697	2.371	0.900	1.00	2.371	–
B	2	42.00	53.85	5.90	6.142	3.518	0.900	1.00	3.518	–
C	7	37.68	34.62	3.79	6.252	4.523	0.961	0.61	4.412	0.0540
D	12	33.30	15.38	1.69	6.523	5.466	0.955	0.26	4.838	0.0540
TOL (E)	-10	55.00	100.00	10.96	8.969	2.113	0.900	1.00	2.113	–
Tbiv (F)	-7	52.00	88.46	9.70	9.697	2.371	0.900	1.00	2.371	–

Adaption of water temperature – according to ČSN EN 14825:2023, Annex E

- Medium temperature application (reference water temperature 55 °C)
- Reference season „A“ – average
- Condition D
- Fixed water flow rate – secondary circuit

General formulas and derivation:

$$\begin{aligned}
 t_{\text{outlet, average}} &= t_{\text{inlet, capacity test}} + (t_{\text{outlet, capacity test}} - t_{\text{inlet, capacity test}}) \cdot CR & [^{\circ}\text{C}] \\
 t_{\text{outlet, average}} &= t_{\text{inlet, capacity test}} + (\Delta t) \cdot CR & [^{\circ}\text{C}] \\
 t_{\text{outlet, average}} &= t_{\text{outlet, capacity test}} - \Delta t + \Delta t \cdot CR & [^{\circ}\text{C}] \\
 t_{\text{outlet, capacity test}} &= t_{\text{outlet, average}} + \Delta t - \Delta t \cdot CR & [^{\circ}\text{C}]
 \end{aligned}$$

For fixed flow:

$$\Delta t = \text{Declared capacity} / \text{Declared capacity}_{\text{standard rating conditions A7W55}} \cdot 8$$

$$CR \cdot \Delta t = \text{Part load} / \text{Declared capacity} \cdot \text{Declared capacity} / \text{Declared capacity}_{\text{standard rating conditions A7W55}} \cdot 8$$

$$CR \cdot \Delta t = \text{Part load} / \text{Declared capacity}_{\text{standard rating conditions A7W55}} \cdot 8$$

$$t_{\text{outlet, capacity test, fixed flow}} = t_{\text{outlet, average}} + \text{Declared capacity} / \text{Declared capacity}_{\text{standard rating conditions A7W55}} \cdot 8 - \text{Part load} / \text{Declared capacity}_{\text{standard rating conditions A7W55}} \cdot 8$$

$$t_{\text{outlet, capacity test, fixed flow}} = t_{\text{outlet, average}} + 8 / \text{Declared capacity}_{\text{standard rating conditions A7W55}} \cdot (\text{Declared capacity} - \text{Part load})$$

Measured data:

$t_{\text{outlet, average}}$	30.00	[°C]
Declared capacity	6.523	[kW]
Declared capacity _{standard rating condition A7W55}	11.721	[kW]
Part load	1.69	[kW]

Calculation of water temperature

$$t_{\text{outlet, capacity test, fixed flow}} = 30 + 8 / 11.721 \cdot (6.523 - 1.690) = \underline{\underline{33.30}} \quad [^{\circ}\text{C}]$$

Calculation SCOP, SCOP_{on}, SCOP_{net}

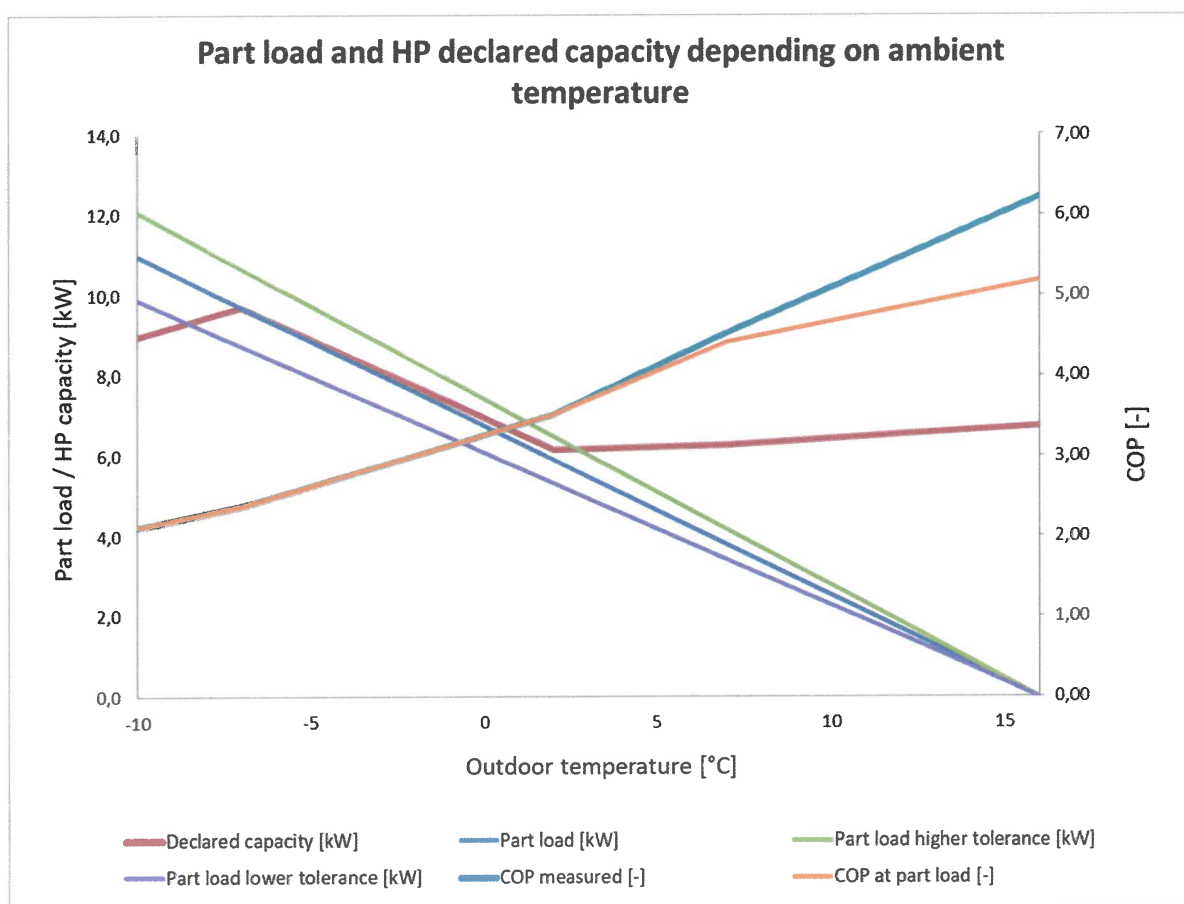
- Medium temperature application (reference water temperature 55 °C)
- Reference heating season „A“ – average

Bin	Outdoor temp. (dry bulb)	Hours	Part load ratio	Heat load	Capacity of HP	Heat load covered by heat pump	Resistive heat elbu (Tj)	Annual resistive heat	COPbin (Tj)	Annual heating demand	Annual power input including electric back up heating	Net annual heating capacity	Net annual power input without electric back up heating
j	Tj	hj		Ph(Tj)			elbu(Tj)	hj x elbu(Tj)	COPbin (Tj)	hj x Ph(Tj)		hj x (Ph(Tj) - elbu(Tj))	
[–]	[°C]	[h]	[%]	[kW]	[kW]	[kW]	[kW]	[kWh]	[–]	[kWh]	[kWh]	[kWh]	[kWh]
TOL(E)	21	-10	1	100.00	10.96	8.97	8.97	1.99	1.99	2.11	11	6	9
	22	-9	25	96.15	10.54	9.21	9.21	1.33	33.22	2.20	264	138	230
	23	-8	23	92.31	10.12	9.45	9.45	0.66	15.28	2.29	233	110	217
A. Tbiv(F)	24	-7	24	88.46	9.70	9.70	9.70	0.00	0.00	2.37	233	98	233
	25	-6	27	84.62	9.28	9.30	9.28	0.00	0.00	2.50	250	100	250
	26	-5	68	80.77	8.85	8.91	8.85	0.00	0.00	2.63	602	229	602
	27	-4	91	76.92	8.43	8.51	8.43	0.00	0.00	2.75	767	279	767
	28	-3	89	73.08	8.01	8.12	8.01	0.00	0.00	2.88	713	247	713
	29	-2	165	69.23	7.59	7.72	7.59	0.00	0.00	3.01	1252	416	1252
	30	-1	173	65.38	7.17	7.33	7.17	0.00	0.00	3.14	1240	395	1240
	31	0	240	61.54	6.75	6.93	6.75	0.00	0.00	3.26	1619	496	1619
	32	1	280	57.69	6.32	6.54	6.32	0.00	0.00	3.39	1771	522	1771
B	33	2	320	53.85	5.90	6.14	5.90	0.00	0.00	3.52	1889	537	1889
	34	3	357	50.00	5.48	6.16	5.48	0.00	0.00	3.70	1957	529	1957
	35	4	356	46.15	5.06	6.19	5.06	0.00	0.00	3.88	1801	465	1801
	36	5	303	42.31	4.64	6.21	4.64	0.00	0.00	4.05	1405	347	1405
	37	6	330	38.46	4.22	6.23	4.22	0.00	0.00	4.23	1391	329	1391
C	38	7	326	34.62	3.79	6.25	3.79	0.00	0.00	4.41	1237	280	1237
	39	8	348	30.77	3.37	6.31	3.37	0.00	0.00	4.50	1174	261	1174
	40	9	335	26.92	2.95	6.36	2.95	0.00	0.00	4.58	989	216	989
	41	10	315	23.08	2.53	6.41	2.53	0.00	0.00	4.67	797	171	797
	42	11	215	19.23	2.11	6.47	2.11	0.00	0.00	4.75	453	95	453
D	43	12	169	15.38	1.69	6.52	1.69	0.00	0.00	4.84	285	59	285
	44	13	151	11.54	1.26	6.58	1.26	0.00	0.00	4.92	191	39	191
	45	14	105	7.69	0.84	6.63	0.84	0.00	0.00	5.01	89	18	89
	46	15	74	3.85	0.42	6.69	0.42	0.00	0.00	5.09	31	6	31
	Σ		4910							Σ	22643	6390	22593

SCOP _{on}	3.54	SCOP _{net}	3.56
		SCOP	3.54

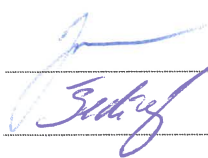
Part load performance diagram

- Medium temperature application (reference water temperature 55 °C)
- Reference heating season „A“ – average



Tested by: Ing. Alexandr Jordanov
Reviewed and approved by: Ing. Dominik Šedivý, Ph.D.

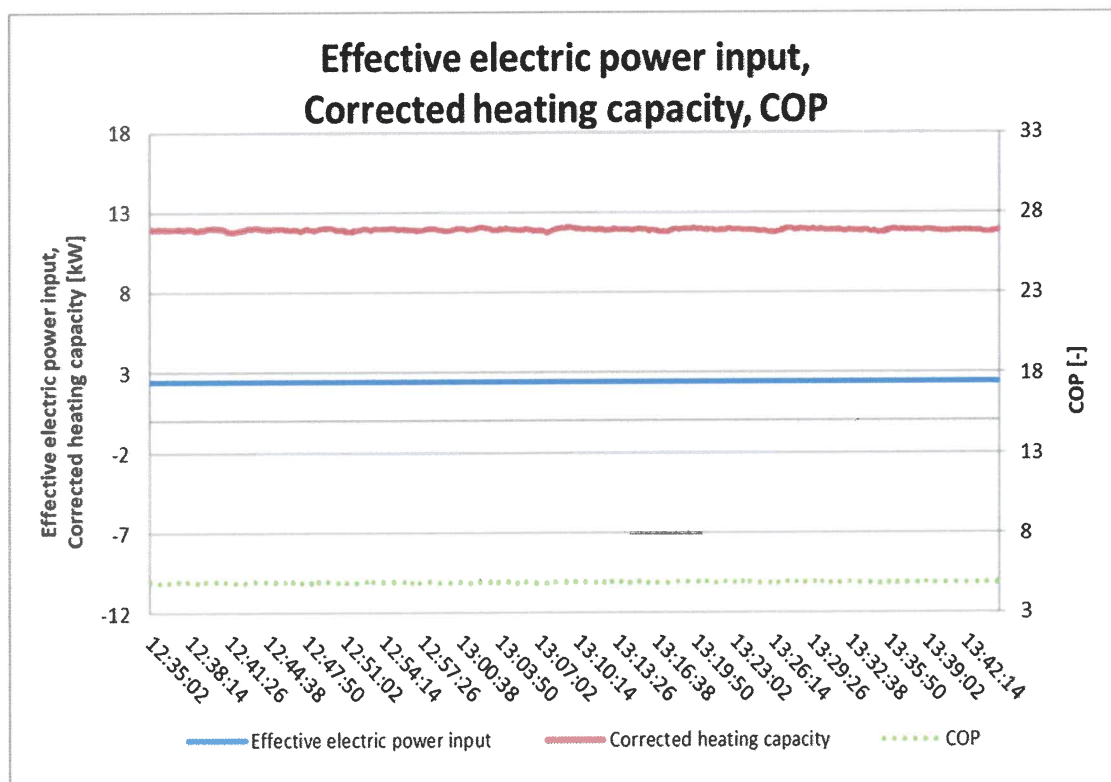
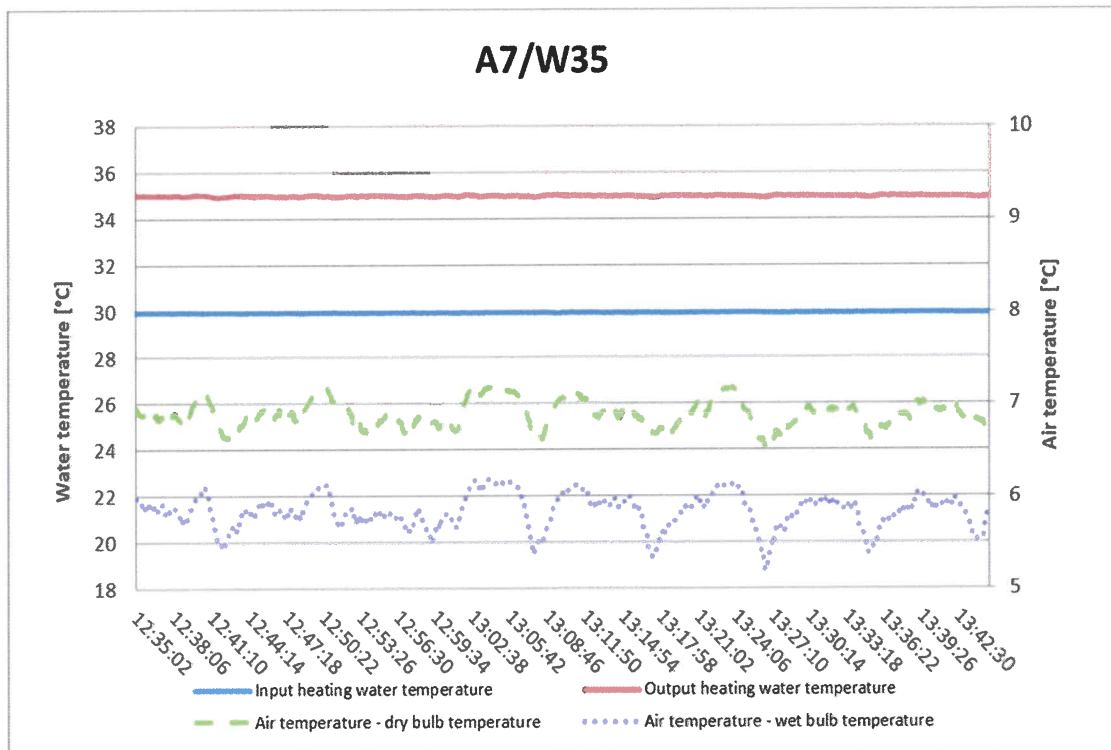
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Date: 2024-08-18

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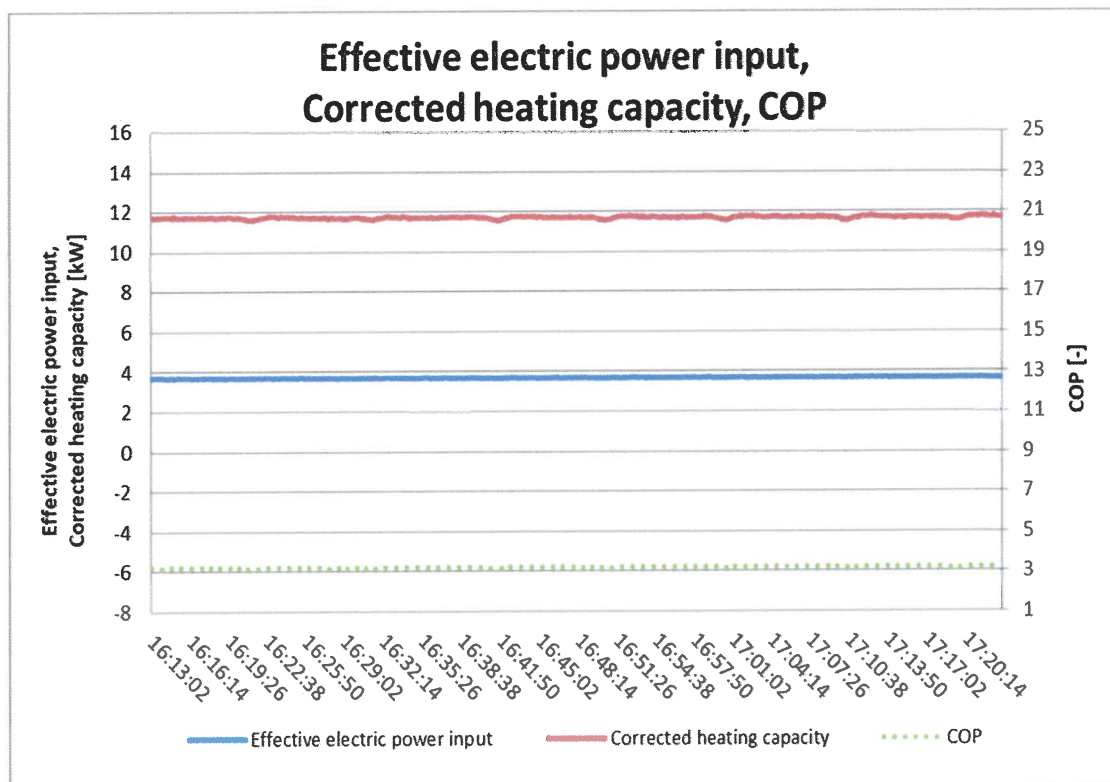
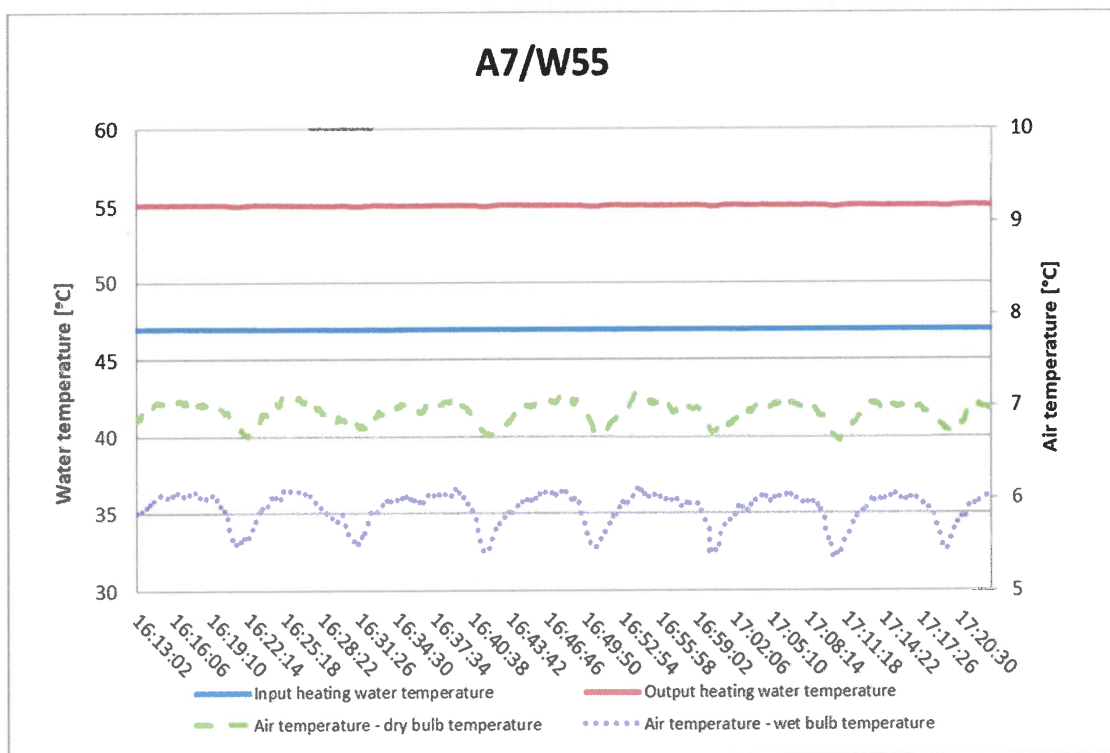
V. Graphs

1. Rating conditions

A7W35 (45 Hz, cp 100%)

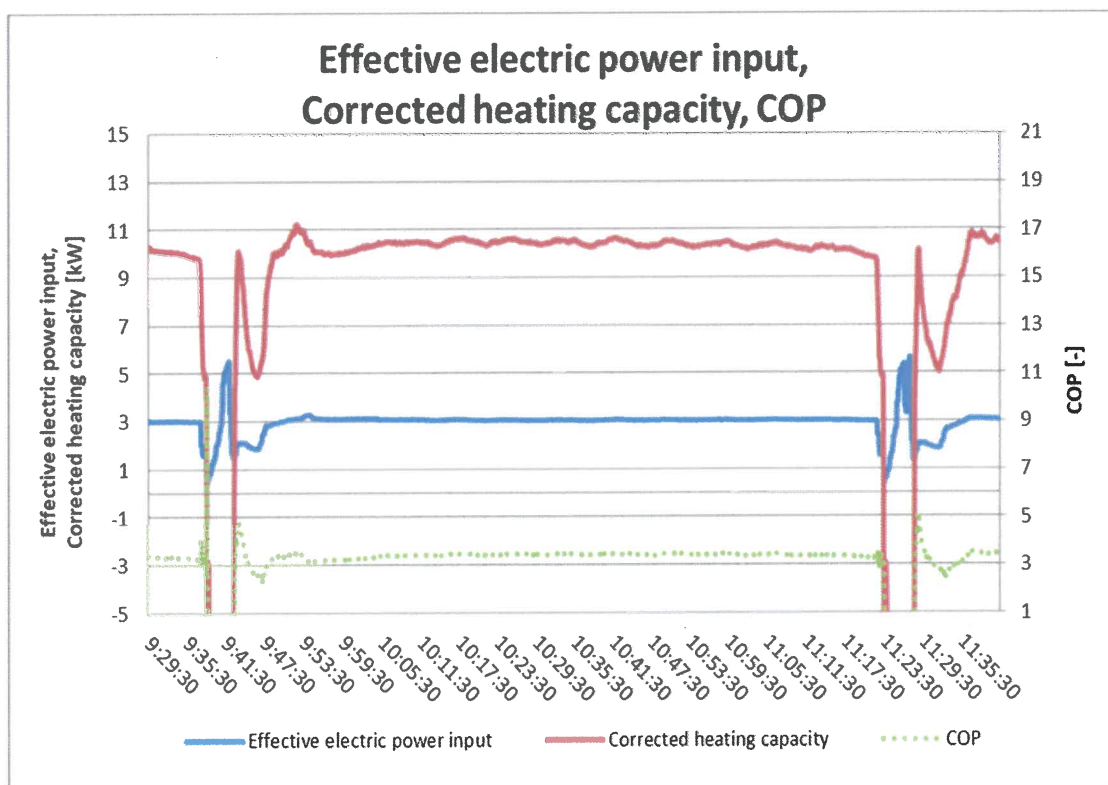
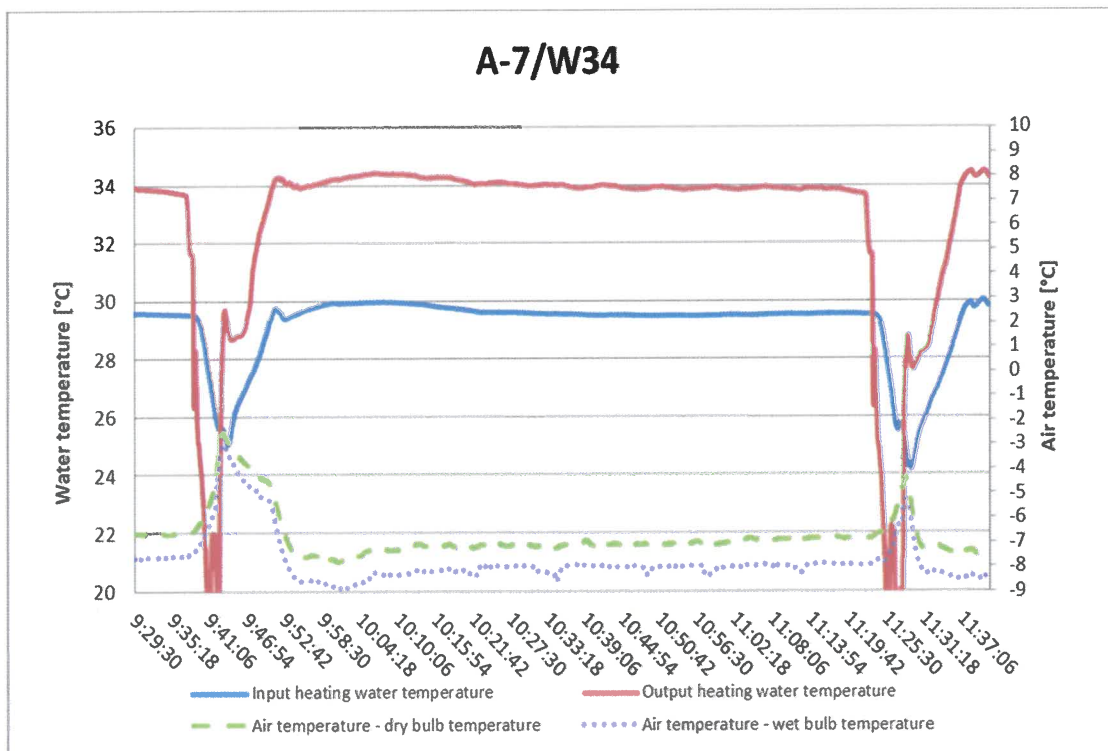


A7W55 (42 Hz, cp 100%)

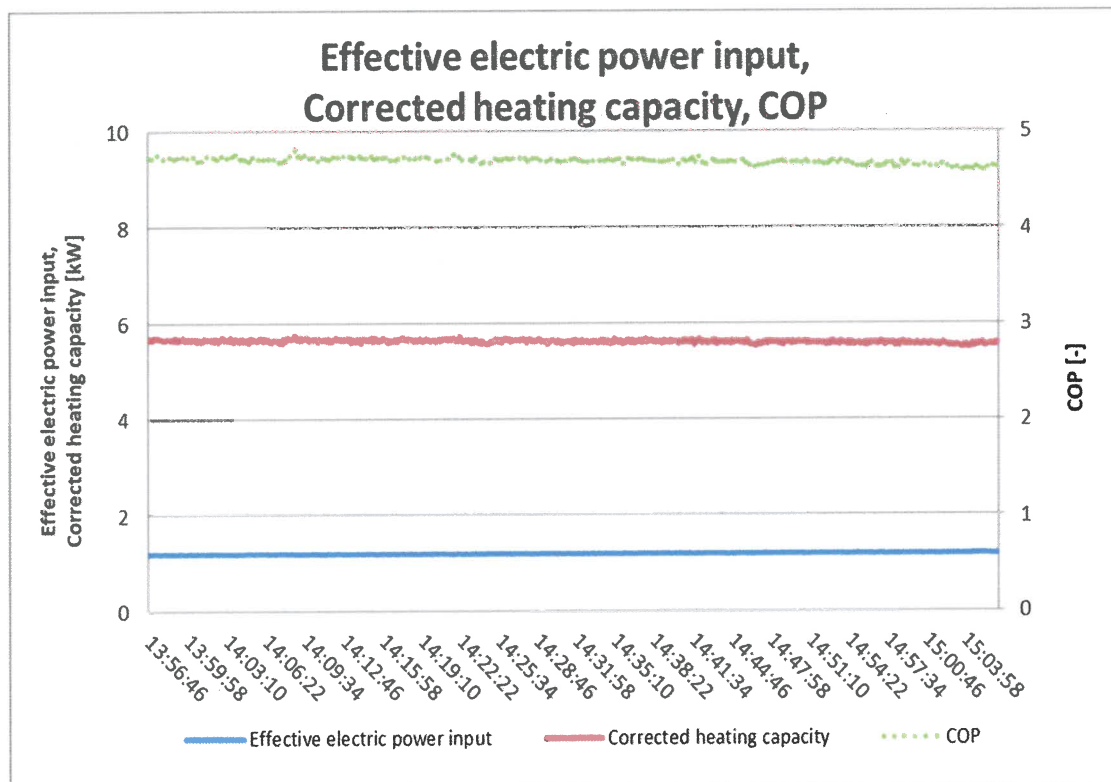
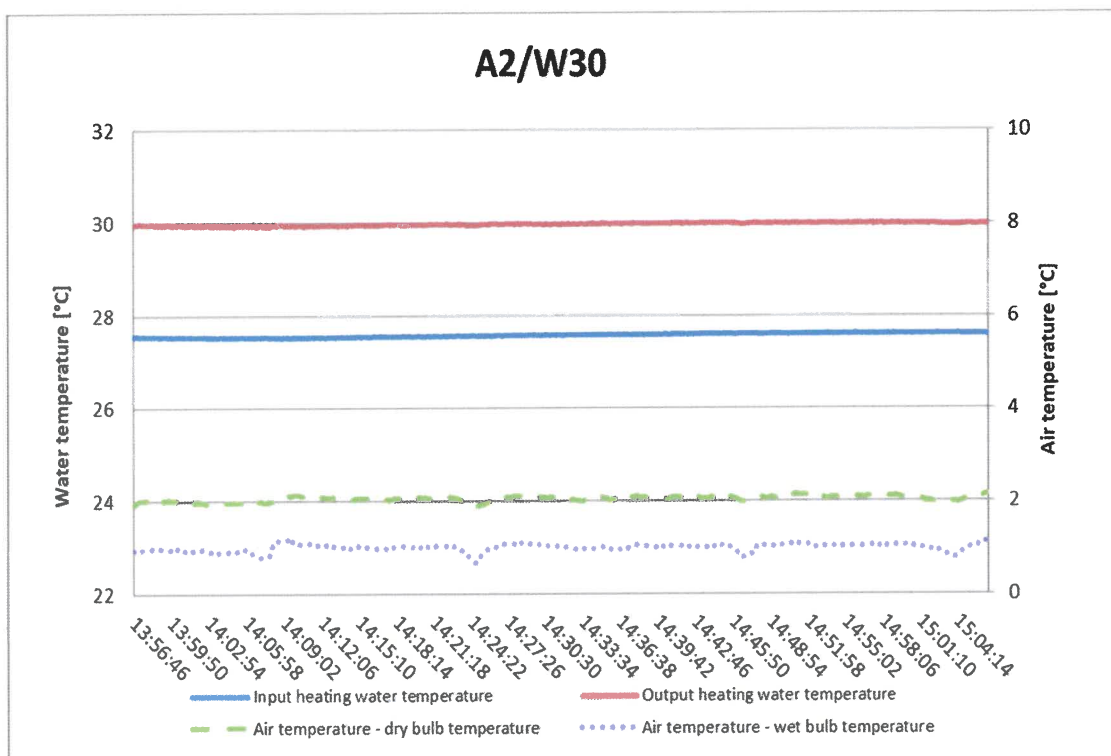


2. Seasonal performance tests and SCOP calculation – Low temperature application

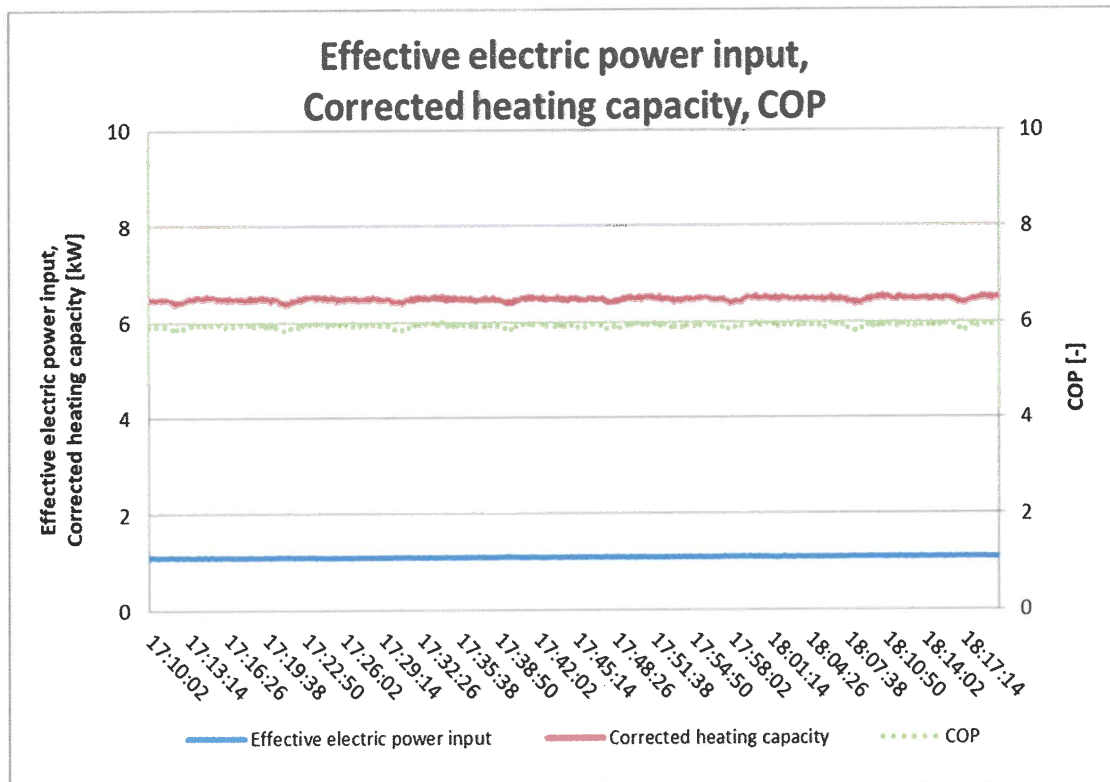
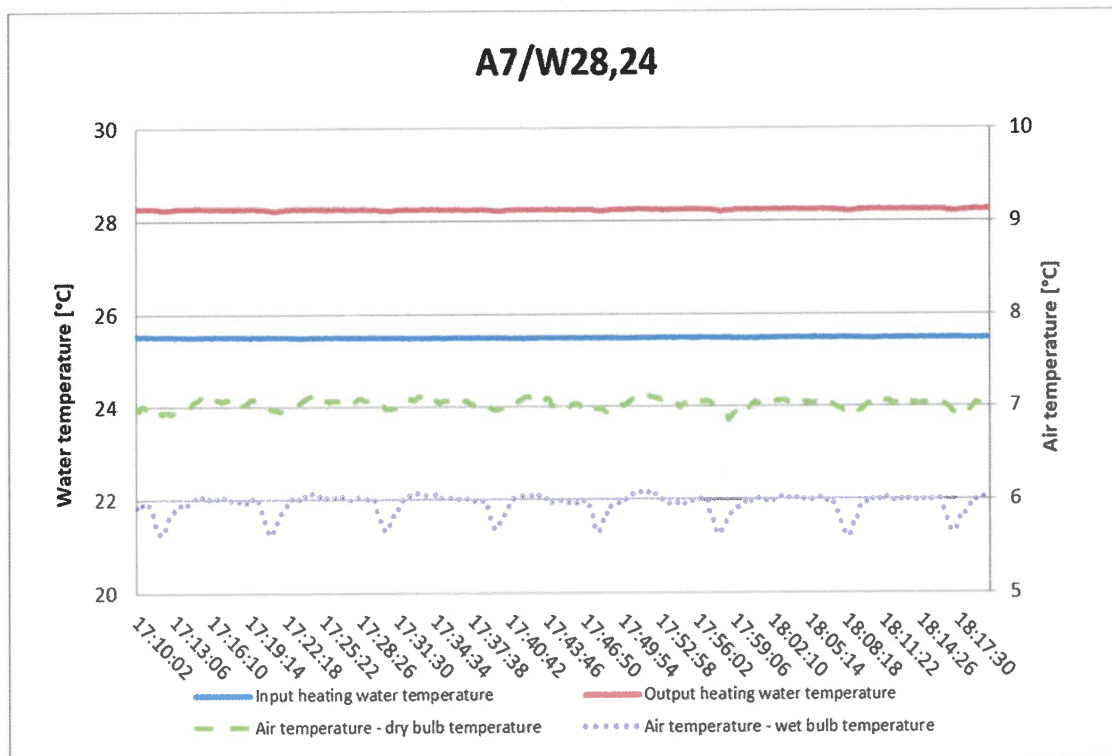
A-7W34 (56 Hz, cp 100%)



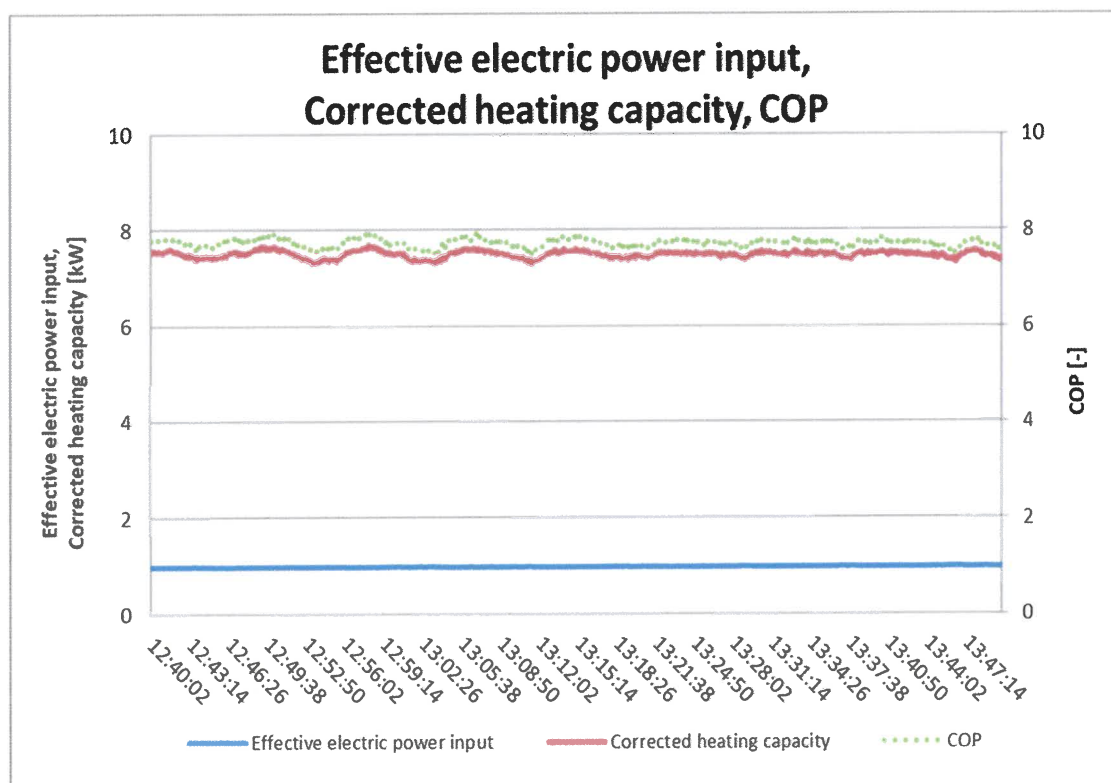
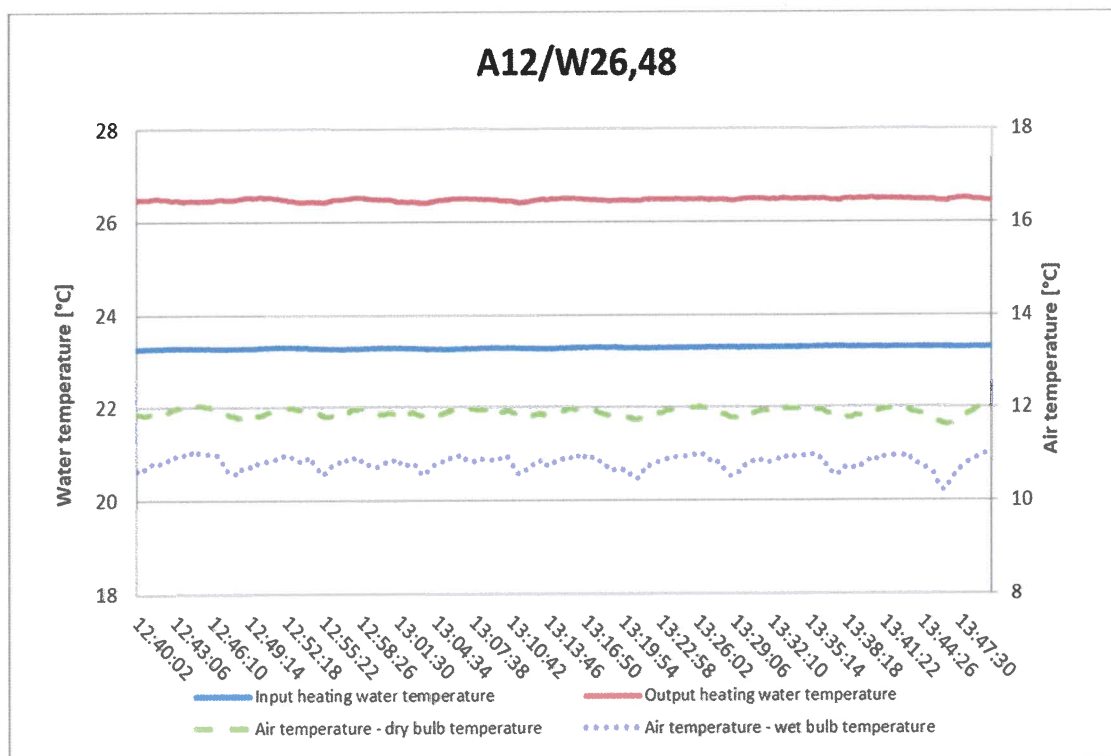
A2W30 (25 Hz, cp 100%)



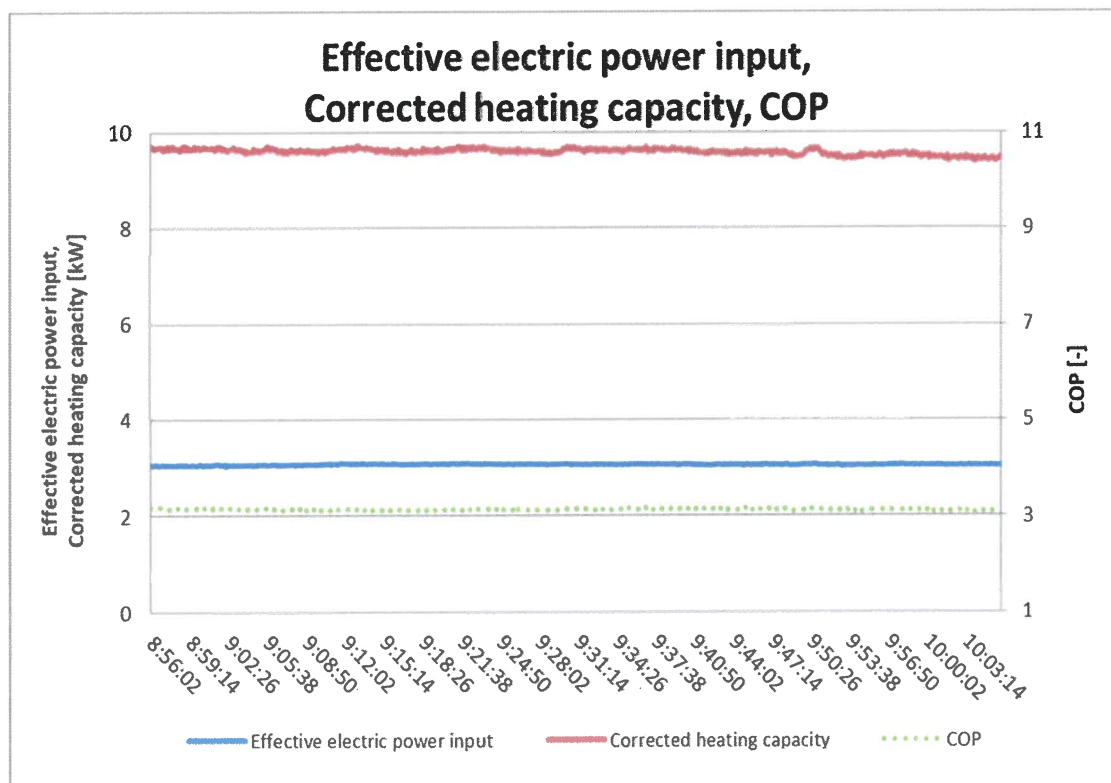
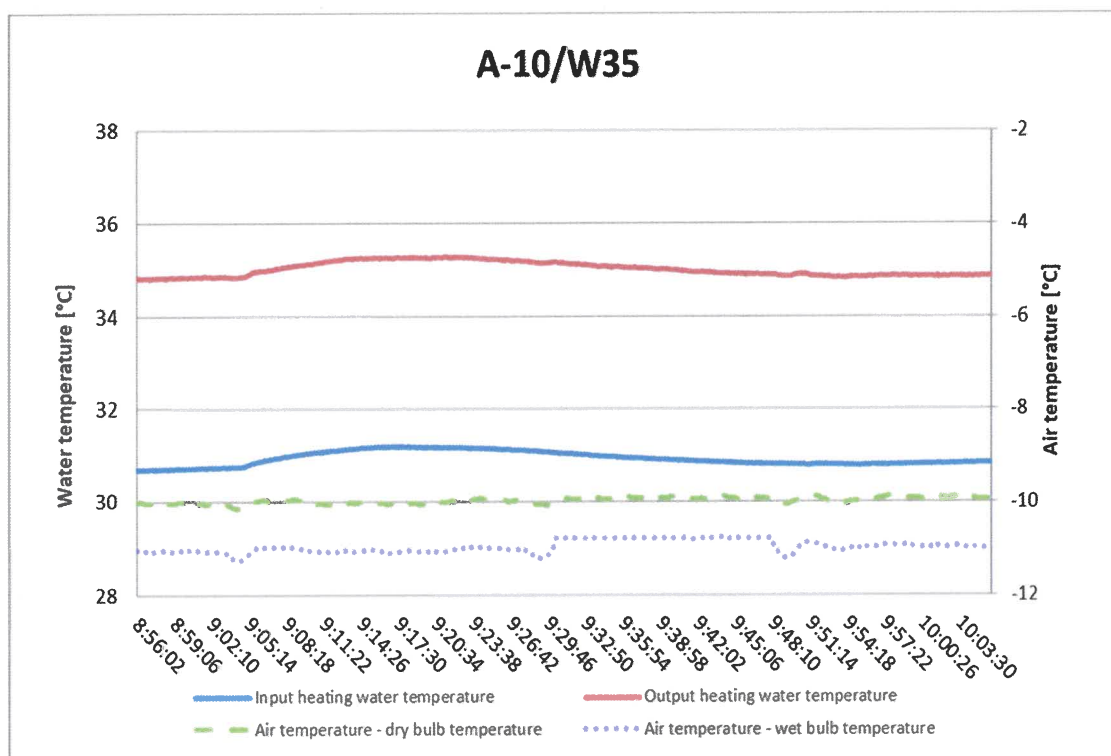
A7W28.24 (25 Hz, cp 100%)



A12W26.48 (25 Hz, cp 100%)

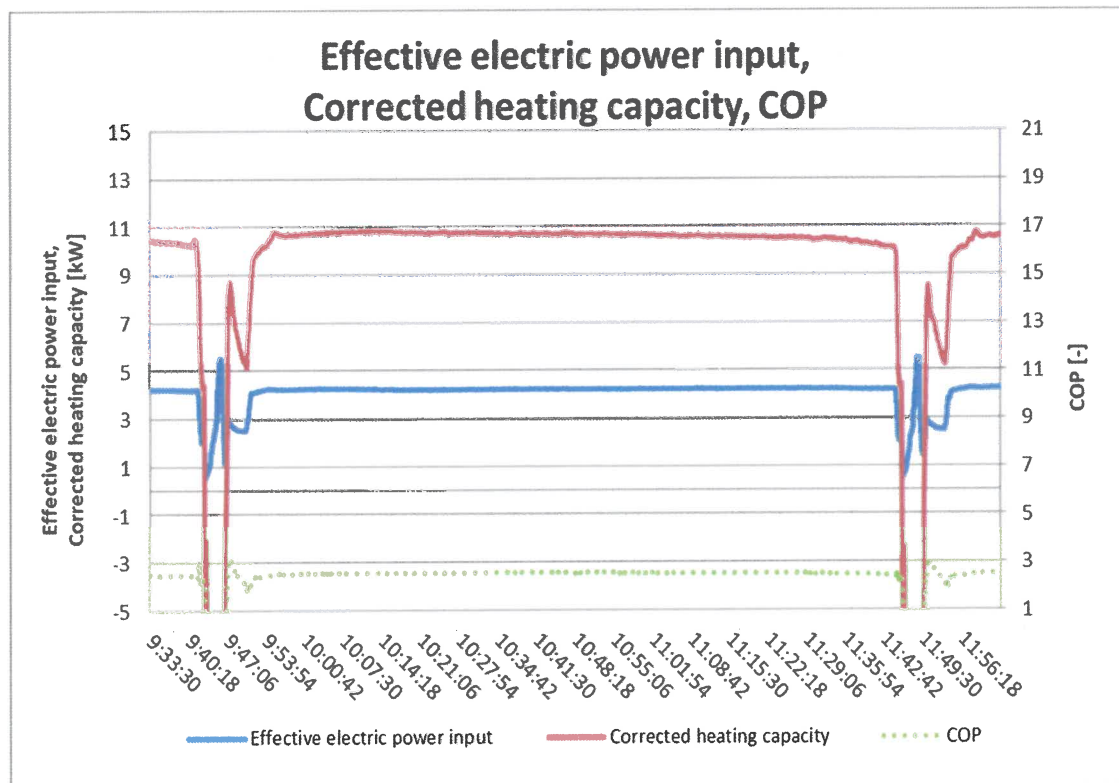
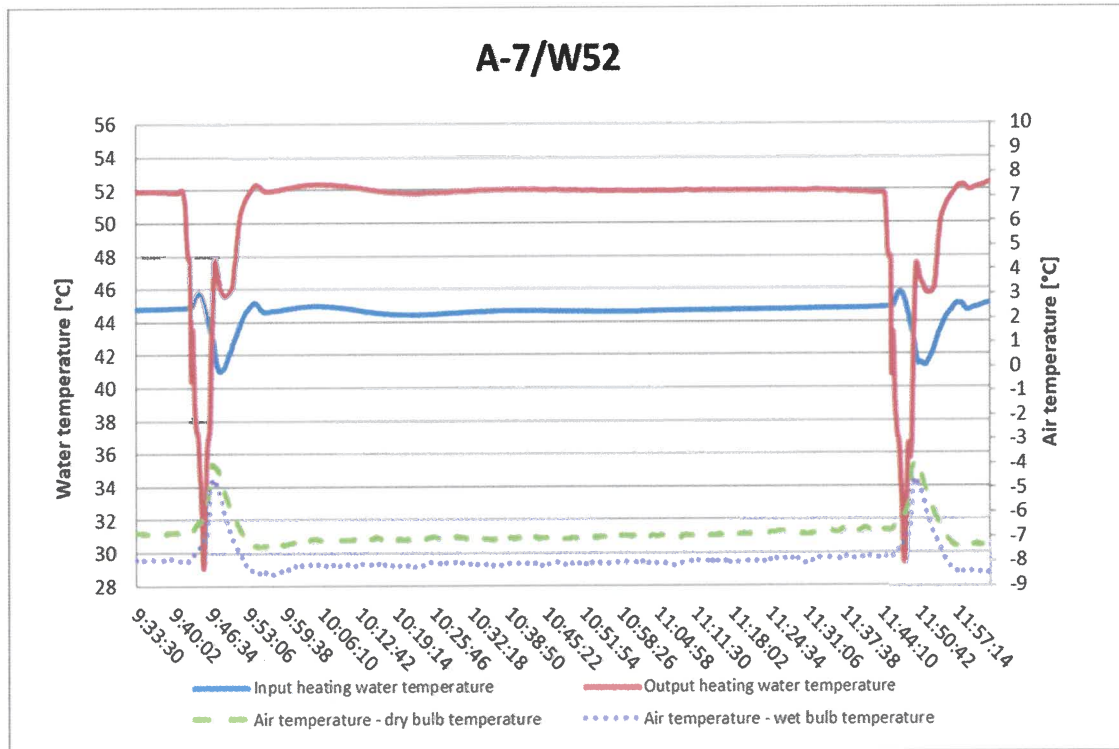


A-10W35 (56 Hz, cp 100%)

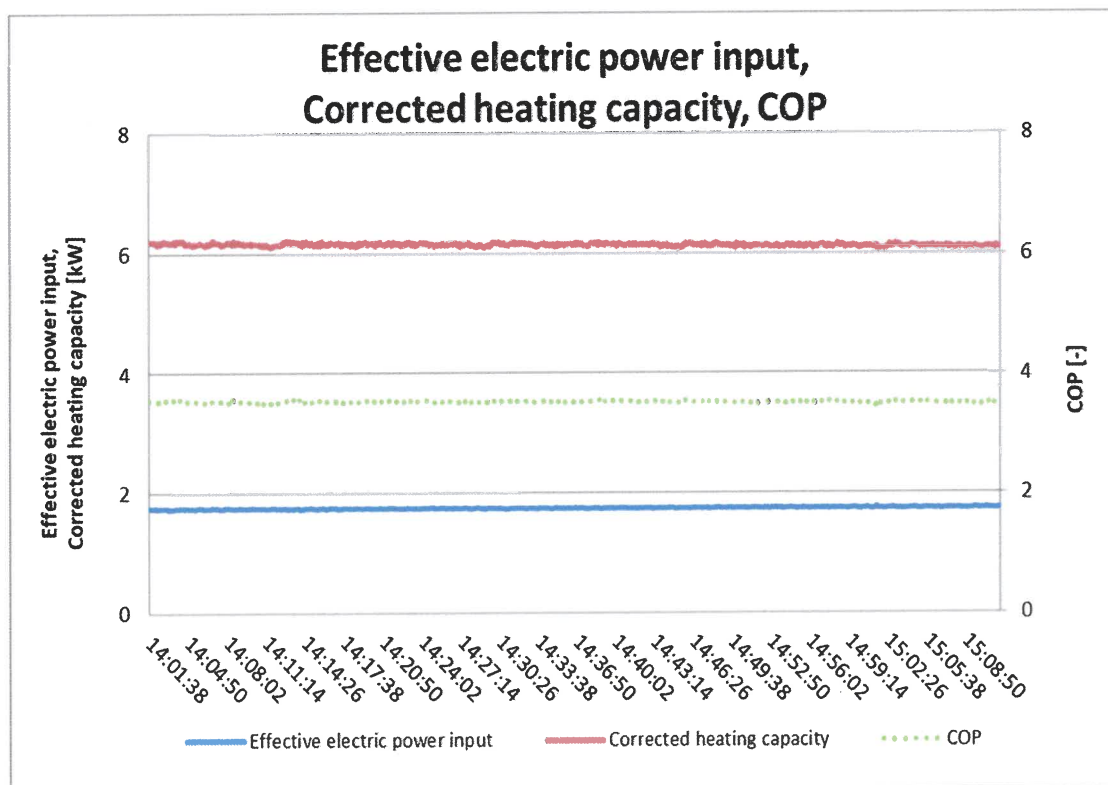
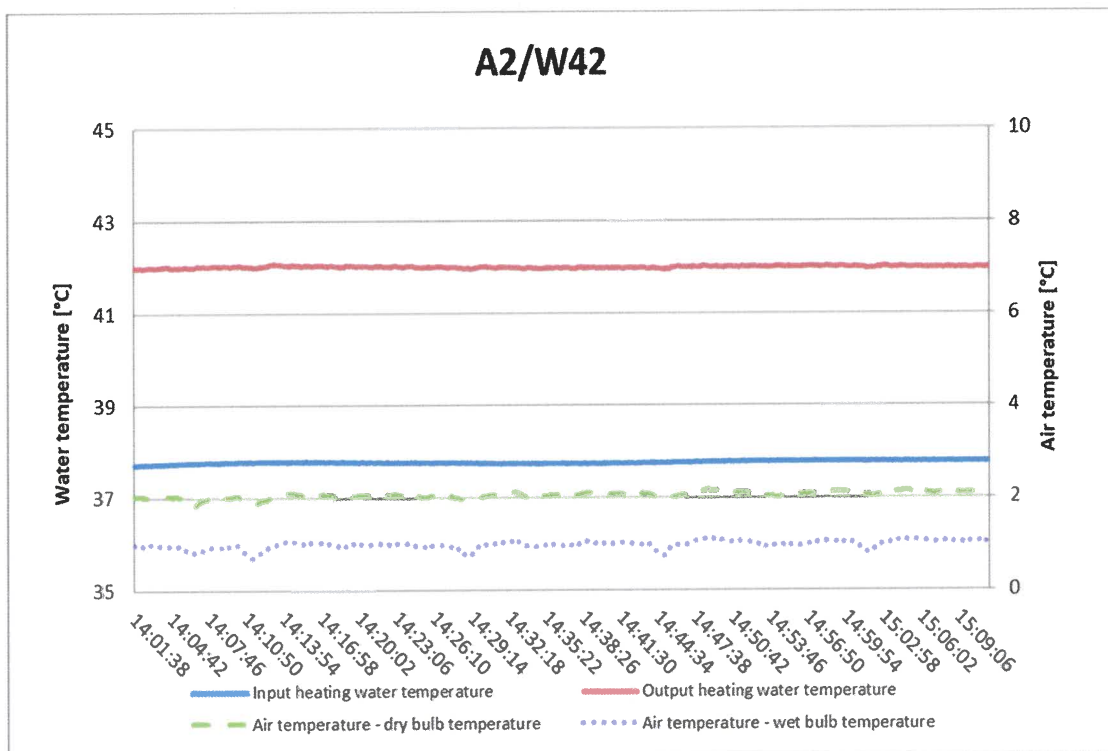


3. Seasonal performance tests and SCOP calculation – Medium temperature application

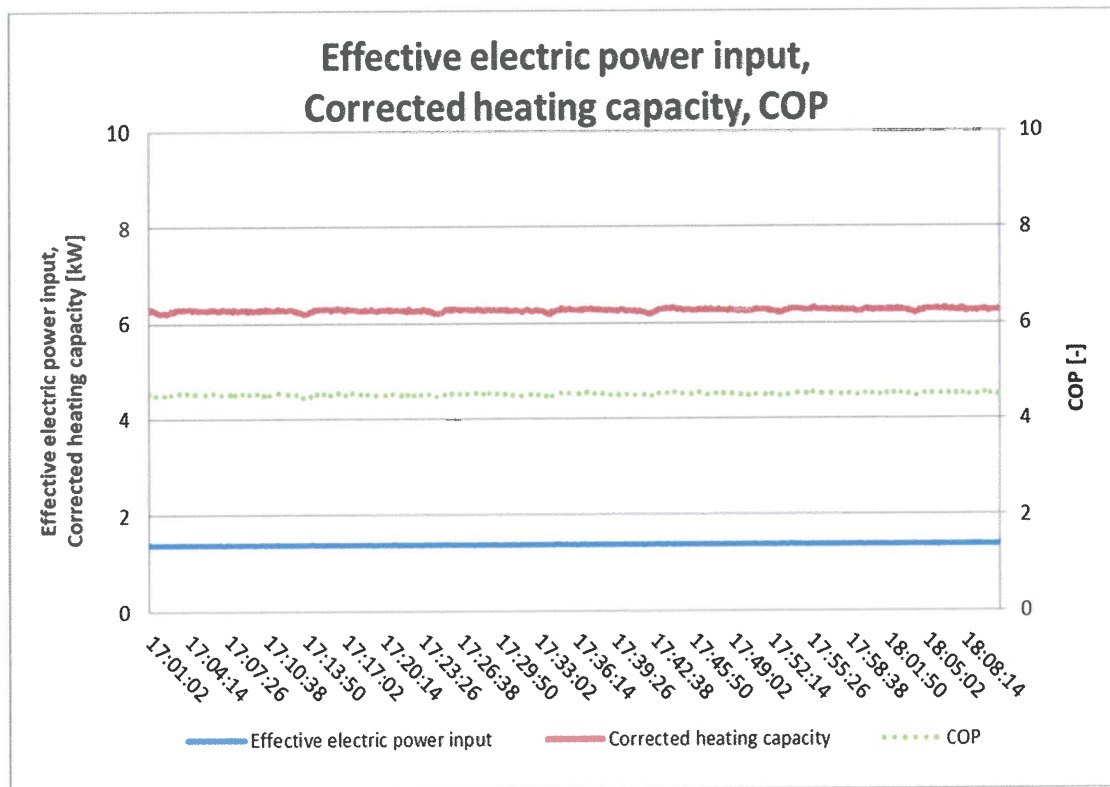
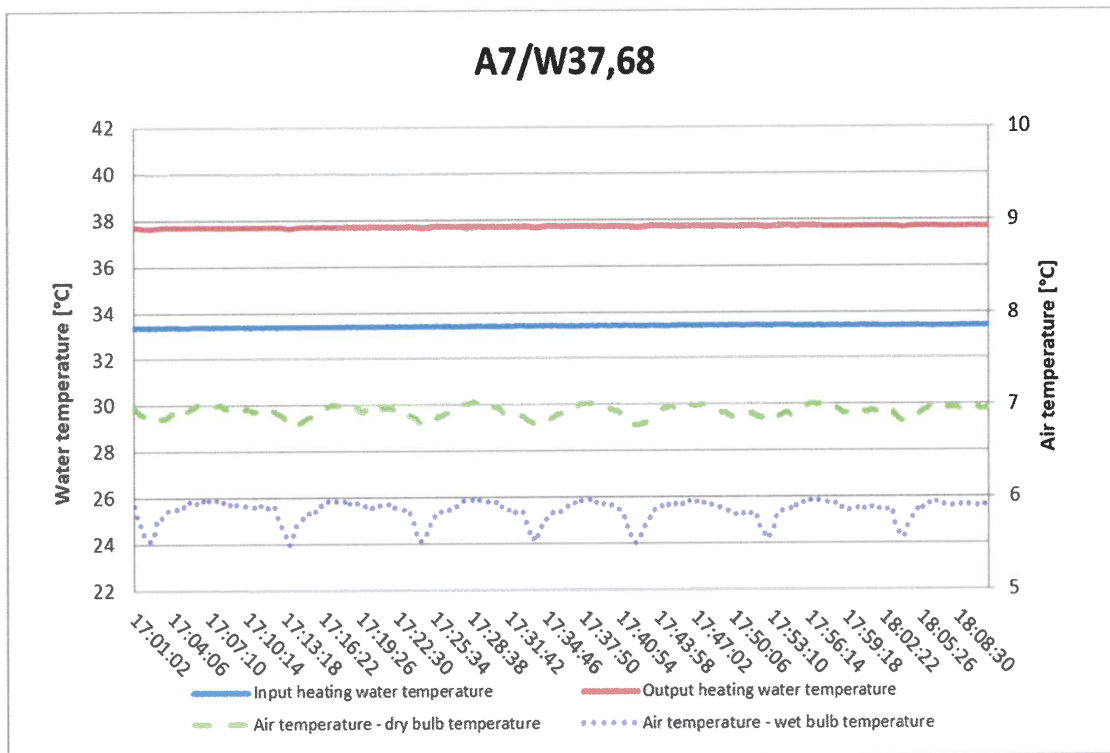
A-7W52 (56 Hz, cp 100%)



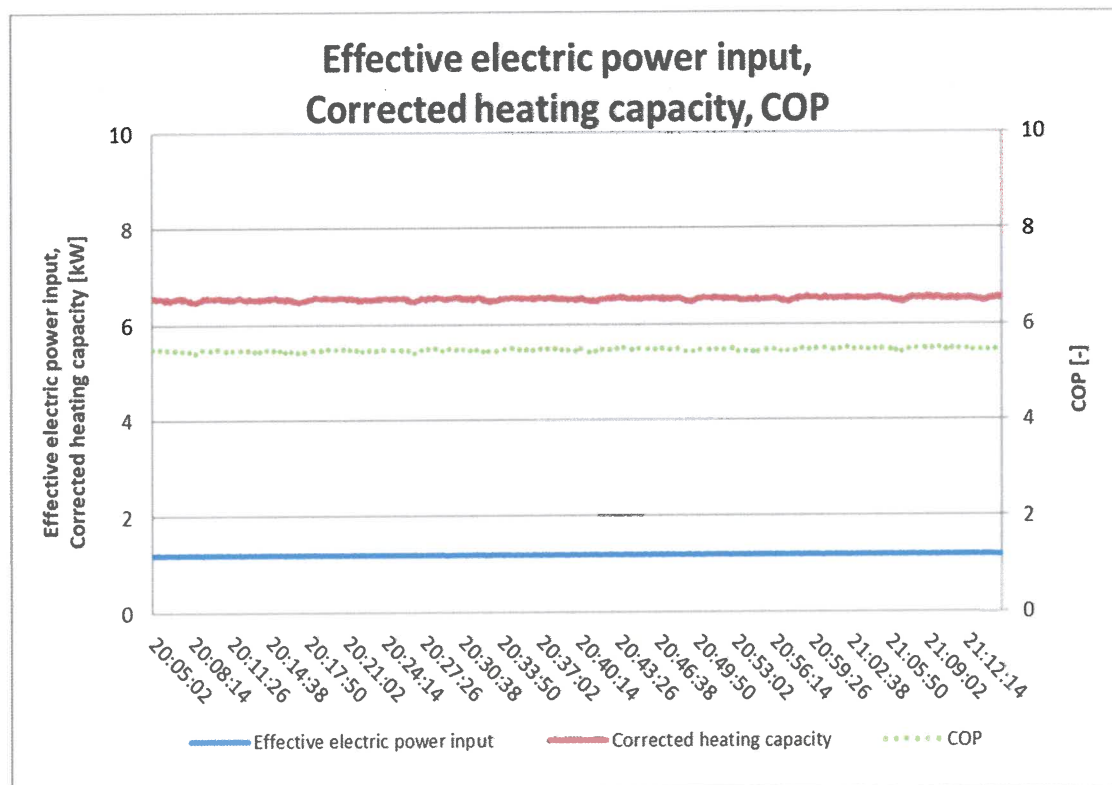
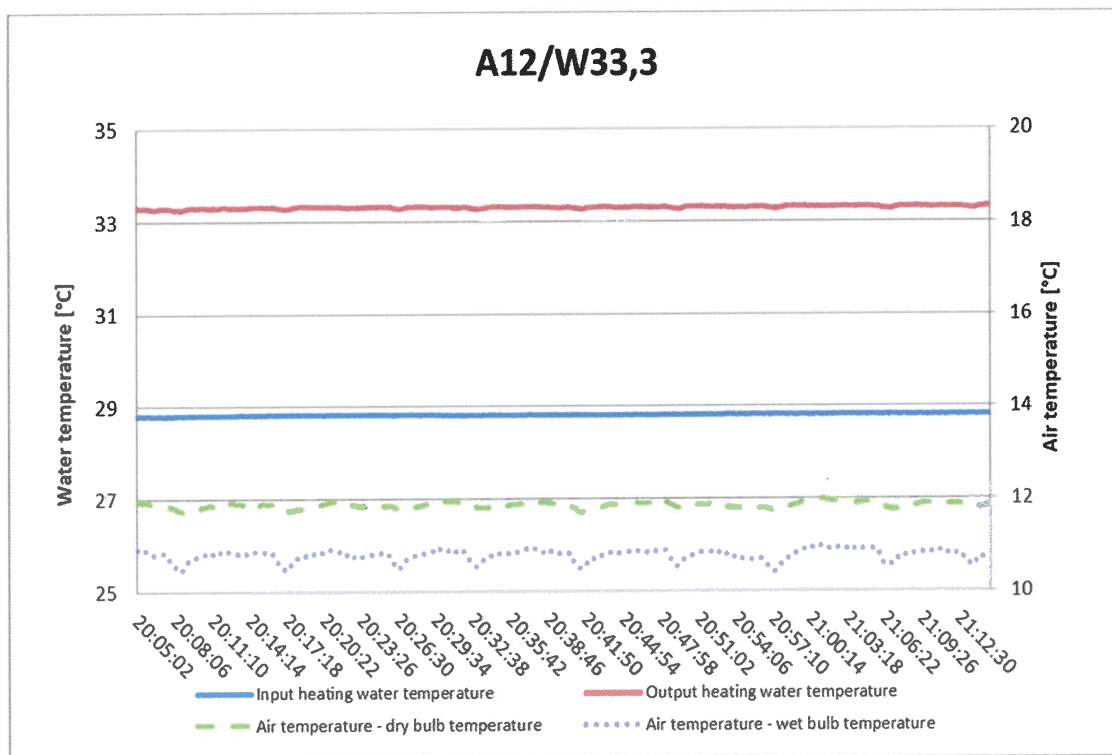
A2W42 (25 Hz, cp 100%)



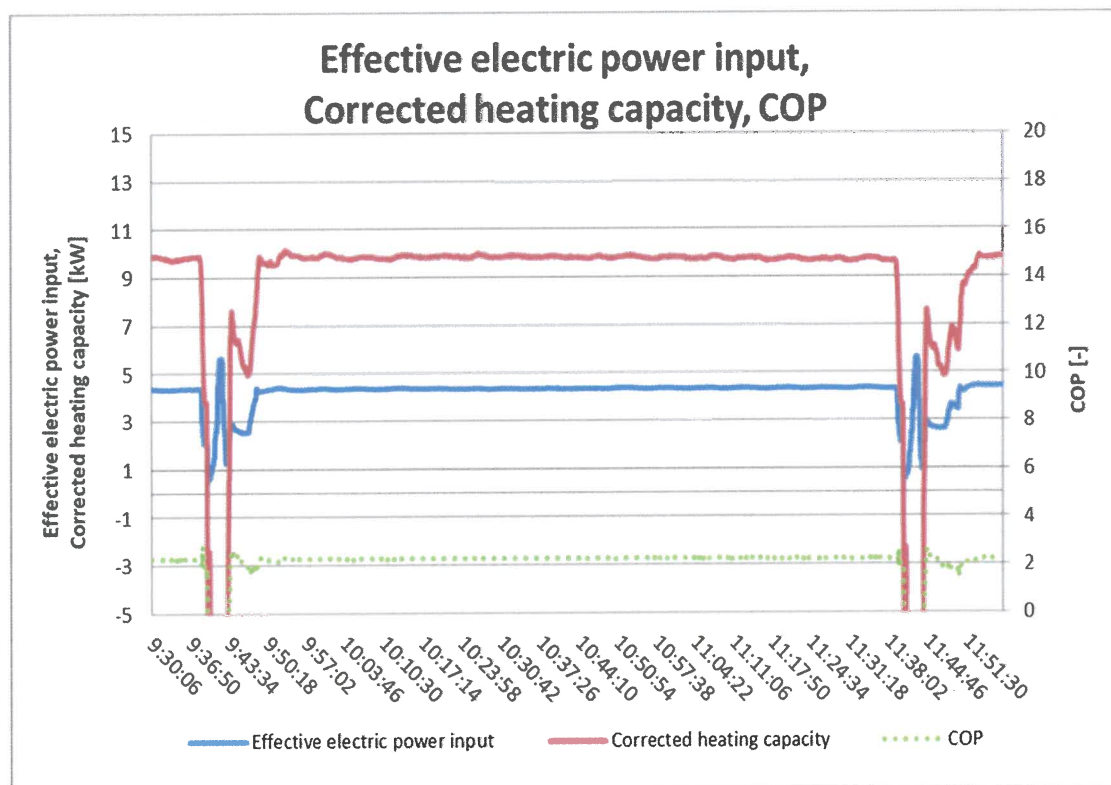
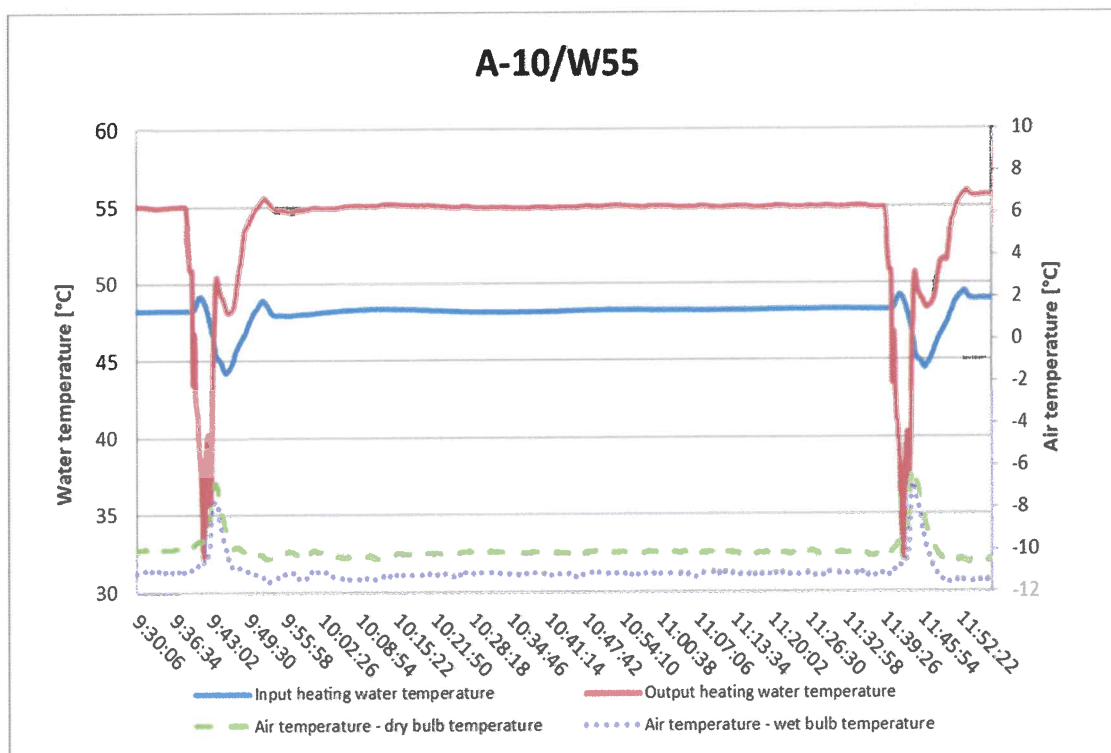
A7W37.68 (25 Hz, cp 100%)



A12W33.30 (25 Hz, cp 100%)



A-10W55 (56 Hz, cp 100%)

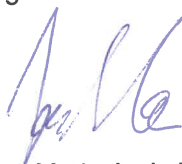


VI. A list of referenced documents

- Order of 2024-05-16 (Order reg. no. B-82250, received on 2024-05-16)
- Contract B-82250/39
- ČSN EN 14511-2:2023 - Air conditioners, liquid chilling packages and heat pumps for space heating and cooling and process chillers, with electrically driven compressors - Part 2: Test conditions
- ČSN EN 14511-3:2023 - Air conditioners, liquid chilling packages and heat pumps for space heating and cooling and process chillers, with electrically driven compressors - Part 3: Test methods
- ČSN EN 14825:2023 - Air conditioners, liquid chilling packages and heat pumps, with electrically driven compressors, for space heating and cooling, commercial and process cooling - Testing and rating at part load conditions and calculation of seasonal performance

Test Report compiled by:

Ing. Alexandr Jordanov



Test Report approved by:

Ing. Mario Jankola
Heating Equipment and Construction Products Manager



– End of Test Report –



mgr Jerzy Podgórski
Tłumacz przysięgły języka angielskiego
ul. Łabiszyńska 17 m. 84, 03-397 Warszawa
Tel. (+48 22) 744 00 66 (biuro),
(+48) 501 211 100

TŁUMACZENIE Z JĘZYKA ANGIELSKIEGO

[dokument sporządzono na papierze firmowym Engineering Test Institute]
[dokument posiada nagłówek w języku angielskim i innym języku obcym o następującej treści:]

Strojírenský zkušební ústav, s.p., Brno, Česká republika
Instytut Badań Technicznych, Przedsiębiorstwo Państwowe, Brno, Republika Czeska

CERTYFIKAT BADAŃ
Numer O-B-01390-24

Klient Guangdong Tongyi Heat Pump Science and Technology Corp.
Room 2001-2010, 20/F, No.159 Middle Qiaozhong Road
510163 Liwan District, Guangzhou
CHINY

Produkt Pompa ciepła powietrze/woda – monoblok

Oznaczenie typu / znak towarowy TAHMV12S A

Metody testowe ČSN EN 14511-2:2023, ČSN EN 14511-3:2023, ČSN EN 14825:2023;
ČSN EN 12102-1:2023

Podstawa certyfikatu Raporty z badań:
39-17758/T z 2024-07-18
39-17758/H z 2024-07-17
Dokumenty techniczne Guangdong Tongyi Heat Pump Science and
Technology Corp.

Referencyjny sezon grzewczy „A” = średnia
(Temperatura projektowa odniesienia $T_{designh} = -10^{\circ}C$)

Wyniki:

NISKA TEMPERATURA

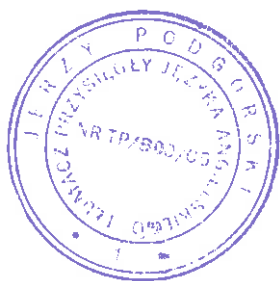
(Referencyjna temperatura wody 35°C)

ŚREDNIA TEMPERATURA

(Referencyjna temperatura wody 55°C)

10,20	P _{designh} [kW] .. Ogrzewanie przy pełnym obciążeniu				10,96
4,66	SCOP [-]... Współczynnik efektywności sezonowej				3,54
Temperatura zewnętrzna	Deklarowana wydajność grzewcza	Współczynnik efektywności przy deklarowanej wydajności	Temperatura zewnętrzna	Deklarowana wydajność grzewcza	Współczynnik efektywności przy deklarowanej wydajności
T _j [°C]	P _{dh} [kW]	COP _d [-]	T _j [°C]	P _{dh} [kW]	COP _d [-]
T _j =-7	9,020	3,015	T _j =-7	9,697	2,371
T _j = +2	5,620	4,692	T _j =+2	6,142	3,518
T _j =+7	6,496	5,925	T _j =+7	6,252	4,523
T _j = +12	7,490	7,727	T _j = +12	6,523	5,466
T _j = TOL = -10	9,589	3,127	T _j = TOL = -10	8,969	2,113
T _j = T _{bivalent} = -7	9,020	3,015	T _j = T _{bivalent} = -7	9,697	2,371

[pieczęć okrągła w innym języku obcym o następującej treści:] Strojírenský zkušební ústav, CZ 1
O-B-01390-24, strona 1 (2)



(Referencyjna temperatura wody 35°C)

Pobór mocy w trybach innych niż „tryb aktywny”:

52,4	Tryb wył.	P_{OFF}	[W]	52,4
53,7	Tryb wył. termostatu	P_{TO}	[W]	54,0
52,4	Tryb czuwania	P_{SB}	[W]	52,4
0,0	Tryb podgrzewacza skrzyni korbowej	P_{CK}	[W]	0,0

Roczne zużycie energii elektrycznej na ogrzewanie wg:

4524	ČSN EN 14825:2023	Q_{HE}	[kWh]	6406
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Sezonowa efektywność energetyczna ogrzewania pomieszczeń

183,2	ČSN EN 14825:2023 η_s [%]	138,6
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Natężenie przepływu cieczy w zewnętrznym wymienniku ciepła:

-	Ciecz źródłowa Min/Max [m³/h]	
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Natężenie przepływu cieczy w wewnętrznym wymienniku ciepła:

2,0536 / 2,0603	Woda grzewcza Min/Max [m³/h]	1,2701 / 1,2788
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Poziom mocy akustycznej w warunkach A7W55* (przy 25 Hz):

TAHMOV12S A

- Jednostka zewnętrzna -

L_{WA}	$56,6 \pm 1,5$	dB(A)
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Klasa dokładności 2
(techniczna)

(*) *Komentarz do skróconego oznaczenia:*

„A” powietrze, „7” temperatura na wlocie (temperatura termometru suchego) w °C, „W” woda, „35” temperatura na wylocie w °C.

Specyfikacja warunków:

Regulacja prędkości sprężarki	Zmienna	Objęściowe natężenie przepływu wody grzewczej (wewnętrzny wymiennik ciepła)	Stale
Temperatura wody na wylocie (wewnętrzny wymiennik ciepła)	Zmienna	Natężenie przepływu objęściowego cieczy źródłowej (zewewnętrzny wymiennik ciepła)	-
Funkcja	Odwracalna		

Instytut Badań Technicznych, Przedsiębiorstwo Publiczne, potwierdza niniejszym Certyfikatem Badań, że badanie danego produktu zostało przeprowadzone z uzyskanymi wynikami podanymi powyżej. Instytut Badań Technicznych, Przedsiębiorstwo Publiczne, jest akredytowanym Laboratorium Badawczym 1045.1.

Brno, 13.08.2024

[pieczęć okrągła w innym języku obcym o następującej treści:] Strojirenský zkušební ústav, CZ 1

[nieczytelny podpis]

Ing. Mario Jankola

Kierownik ds. urządzeń grzewczych i wyrobów budowlanych
- KONIEC CERTYFIKATU BADAŃ -

O-B-01390-24, strona 2 (2)

XX

Ja, Jerzy Podgórski, tłumacz przysięgły języka angielskiego wpisany na listę tłumaczy przysięgłych Ministra Sprawiedliwości RP pod numerem TP/800/05, zaświadczam zgodność powyższego tłumaczenia z wersją PDF dokumentu sporządzonego w języku angielskim.

Warszawa, 20 września 2024 roku, Nr Rep.721



OŚWIADCZENIE

Guangdong Tongyi Heat Pump Science and
Technology Corp. oświadcza, iż pompy ciepła

- 1) TAHMV9S A
Oznaczenie/typ/identyfikator modelu
- 2) TAHMV12S A
Oznaczenie/typ/identyfikator modelu
- 3) TAHMV14S A
Oznaczenie/typ/identyfikator modelu
- 4) TAHMV16S A
Oznaczenie/typ/identyfikator modelu
- 5)
Oznaczenie/typ/identyfikator modelu

Należą do jednego podtypu w danym typoszeregu i spełniają łącznie następujące warunki:

- identyczna konstrukcja obiegu chłodniczego, ten sam czynnik chłodniczy/roboczy;
- ten sam producent, typ i liczba sprężarek;
- ten sam typ elementu rozprężnego;
- ten sam typ skraplacza;
- ten sam typ parownika;
- ten sam typ procesu odszraniania;
- ten sam sterownik i zasada sterowania wydajnością;
- ten sam producent, typ i liczba wentylatorów parownika (w przypadku powietrznych pomp ciepła) i zasada sterowania wydajnością (stała, zmienna lub stopniowana regulacja prędkości obrotowej);
- urządzenia z i bez zaworu czterodrogowego nie mogą być zaliczone do tego samego typoszeregu.

Guangzhou 2024.9.4

Miejscowość, data


Podpis osoby upoważnionej

